

**Example 13.1 : Page 400**

Reinforced Concrete - Design Theory and Examples

Second Edition

T.J. Macginley &amp; B.S. Choo

appVersion(-4) = "0.99.7822.147"

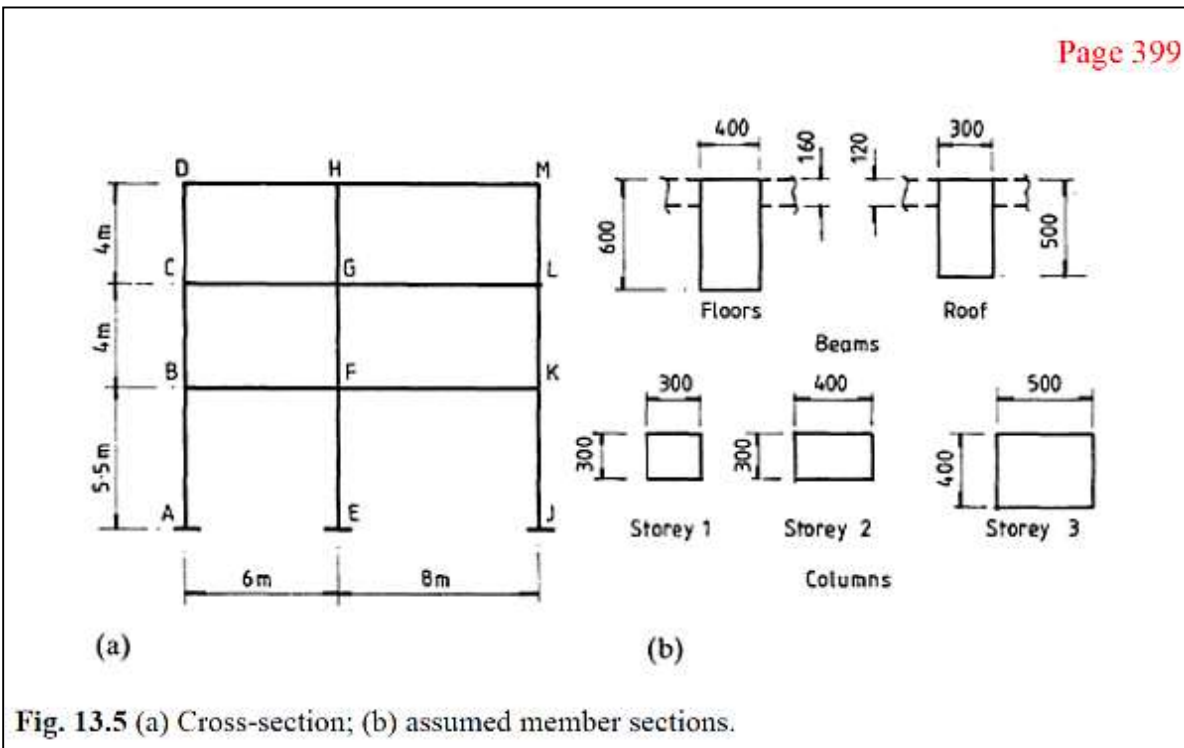
appVersion(4) = "0.99.7822.147"

 $t_0 := \text{time}(0)$ [https://www.academia.edu/34894173/Reinforced\\_Concrete\\_Design\\_Theory\\_and\\_Examples](https://www.academia.edu/34894173/Reinforced_Concrete_Design_Theory_and_Examples)**Example 13.1 Simplified analysis of concrete framed building—vertical load**

The application of the various simplified methods of analysis given in section 3.2 of the code is shown in the following example.

**(a) Specification**

The cross-section of a reinforced concrete building is shown in Fig. 13.5(a). The frames are at 4.5 m centres, the length of the building is 36 m and the column bases are fixed. Preliminary sections for the beams and columns are shown in Fig. 13.5(b). The floor and roof slabs are **designed to span one way** between the frames. Longitudinal beams are provided between external columns of the roof and floor levels only.:



Frames are spaced at 4.5 m

$$\begin{aligned} S_{\text{frame}} &:= 4.5 \text{ m} \\ L_{\text{building}} &:= 36 \text{ m} \\ Y_{\text{cu}} &:= 24 \frac{\text{kN}}{\text{m}^3} \end{aligned}$$

For column GF

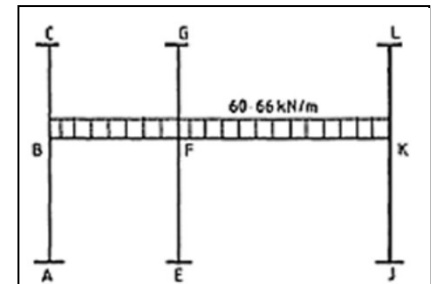
$$\begin{aligned} L_{BF} &:= 6 \text{ m} \\ L_{FK} &:= 8 \text{ m} \end{aligned}$$

**This worked example shows only the analysis of the sub-frame shown. Hence, only Dead & Imposed loads on Beams BF & FK are considered.**

**More Iterations -----> more accuracy**

Number of iterations for Moment Iterations

$$N_{\text{Iter1}} := 3$$



$$\begin{aligned} \begin{bmatrix} col_{FE_b} & col_{FE_h} \\ col_{GF_b} & col_{GF_h} \\ beam_{FK_b} & beam_{FK_h} \end{bmatrix} &:= \begin{bmatrix} 400 \text{ mm} & 500 \text{ mm} \\ 300 \text{ mm} & 400 \text{ mm} \\ 400 \text{ mm} & 600 \text{ mm} \end{bmatrix} \end{aligned}$$

## Loadings

For the floors

Floors D/L

$$g_{k\_floor} := 6.2 \frac{\text{kN}}{\text{m}^2}$$

Floors I/L

$$q_{k\_floor} := 3.0 \frac{\text{kN}}{\text{m}^2}$$

Following load cases are required for the beam **BFK** for the braced frame. But, only **Case 1** is shown in this example.

Case 1  $1.4 \cdot G_k + 1.6 \cdot Q_k$  on the whole beam

Case 2  $1.4 \cdot G_k + 1.6 \cdot Q_k$  on BF and  $1.6 \cdot G_k$  on FK

Case 3  $1.0 \cdot G_k$  on BF and  $1.4 \cdot G_k + 1.6 \cdot Q_k$  on FK

## Loads on Beams

Dead loads on Beams

$$G_{k\_floor} := g_{k\_floor} \cdot S_{frame} = 27.9 \frac{\text{kN}}{\text{m}}$$

Imposed loads on Beams

$$Q_{k\_floor} := q_{k\_floor} \cdot S_{frame} = 13.5 \frac{\text{kN}}{\text{m}}$$

## Calculation of Moments of Inertia

$$I_{Col\_FE} := \frac{1}{12} \cdot col_{FE\_b} \cdot (col_{FE\_h})^3 = 4.1667 \cdot 10^9 \text{ mm}^4$$

$$I_{Col\_FG} := \frac{1}{12} \cdot col_{GF\_b} \cdot (col_{GF\_h})^3 = 1.6 \cdot 10^9 \text{ mm}^4$$

$$I_{beam\_FK} := \frac{1}{12} \cdot beam_{FK\_b} \cdot (beam_{FK\_h})^3 = 7.2 \cdot 10^9 \text{ mm}^4$$

$$I_{beam\_FB} := I_{beam\_FK} = 7.2 \cdot 10^9 \text{ mm}^4$$

Beam BF and FK : same cross section

Moment of Inertia

$$I := \begin{bmatrix} I_{Col\_FE} \\ I_{Col\_FG} \\ I_{beam\_FK} \\ I_{beam\_FB} \end{bmatrix} = \begin{bmatrix} 4.1667 \cdot 10^9 \\ 1.6 \cdot 10^9 \\ 7.2 \cdot 10^9 \\ 7.2 \cdot 10^9 \end{bmatrix} \text{ mm}^4$$

Length  
Cols & Beams

$$L := \begin{bmatrix} 5500 \\ 4000 \\ 8000 \\ 6000 \end{bmatrix} \text{ mm}$$

Stiffness

$$\begin{bmatrix} K_{FE} \\ K_{FG} \\ K_{FK} \\ K_{FB} \end{bmatrix} := \frac{\vec{I}}{L} = \begin{bmatrix} 7.5758 \\ 4 \\ 9 \\ 12 \end{bmatrix} 10^5 \text{ mm}^3$$

## (d) : Subframe analysis for braced frames

The subframe consists of the beams at first floor level and the columns above and below that level with ends fixed.

The frame is analysed for the dead and imposed load cases given in above.

The distribution factors at the joints of the subframe are, for joint **B, F, K** are as follows

### Distribution Factors at the joints of the subframe for

Joint **B**

$$K_B := \begin{bmatrix} K_{FG} \\ K_{FB} \\ K_{FE} \end{bmatrix} = \begin{bmatrix} 4 \\ 12 \\ 7.5758 \end{bmatrix} 10^5 \text{ mm}^3$$

Joint **F**

$$K_F := \begin{bmatrix} K_{FE} \\ K_{FG} \\ K_{FK} \\ K_{FB} \end{bmatrix} = \begin{bmatrix} 7.5758 \\ 4 \\ 9 \\ 12 \end{bmatrix} 10^5 \text{ mm}^3$$

Joint **K**

$$K_K := \begin{bmatrix} K_{FG} \\ K_{FK} \\ K_{FE} \end{bmatrix} = \begin{bmatrix} 4 \\ 9 \\ 7.5758 \end{bmatrix} 10^5 \text{ mm}^3$$

$$K_{B\_tot} := \sum K_B = 2.36 \cdot 10^6 \text{ mm}^3 \quad K_{F\_tot} := \sum K_F = 32.58 \cdot 10^5 \text{ mm}^3 \quad K_{KF\_tot} := \sum K_K = 20.58 \cdot 10^5 \text{ mm}^3$$

$$D_{BC} := \frac{K_{FG}}{K_{B\_tot}} = 0.17$$

$$D_{FE} := \frac{K_{FE}}{K_{F\_tot}} = 0.23$$

$$D_{KL} := \frac{K_{FG}}{K_{KF\_tot}} = 0.19$$

$$D_{BF} := \frac{K_{FB}}{K_{B\_tot}} = 0.51$$

$$D_{FG} := \frac{K_{FG}}{K_{F\_tot}} = 0.12$$

$$D_{KF} := \frac{K_{FK}}{K_{KF\_tot}} = 0.44$$

$$D_{BA} := \frac{K_{FE}}{K_{B\_tot}} = 0.32$$

$$D_{FK} := \frac{K_{FK}}{K_{F\_tot}} = 0.28$$

$$D_{KJ} := \frac{K_{FE}}{K_{KF\_tot}} = 0.37$$

$$D_{FB} := \frac{K_{FB}}{K_{F\_tot}} = 0.37$$

Sanity check

$$D_{BC} + D_{BF} + D_{BA} = 1$$

Sanity check

$$D_{FE} + D_{FG} + D_{FK} + D_{FB} = 1$$

Sanity check

$$D_{KL} + D_{KF} + D_{KJ} = 1$$

## Fixed End Moments

### Case I

### Case II (Not considered in this example)

The FEMs are for case1 (F1) for both beams

$$F1 := 1.4 \cdot G_{k\_floor} + 1.6 \cdot Q_{k\_floor} = 60.66 \frac{\text{kN}}{\text{m}}$$

$$F2 := 1.0 \cdot G_{k\_floor} = 27.9 \frac{\text{kN}}{\text{m}}$$

FEM for span BF: Case I

$$FEM_{BF} := -F1 \cdot \frac{L_{BF}^2}{12} = -181.98 \text{ kN m}$$

FEM for span FK: Case I

$$FEM_{FK} := -F1 \cdot \frac{L_{FK}^2}{12} = -323.52 \text{ kN m}$$

FEM for FB: Case I

$$FEM_{FB} := -FEM_{BF} = 181.98 \text{ kN m}$$

FEM for span KF: Case I

$$FEM_{KF} := -FEM_{FK} = 323.52 \text{ kN m}$$

These programs in Yellow Color) are applicable to any Moment Distribution Method used below

To find column totals

```
tot_BMM(M#) := j := [1..cols(M#)]
               A# j := ∑ col(M#, j)
```

To stack nested matrix

```
Stack_M(M) := A := M_1
               for j ∈ [2..rows(M)]
                 A := stack(A, M_j)
               A
```

$N_{Iter1} = 3$

$N_{Iter2} := 6$

Arrange result matrix for Table

```
Arrange(d, fem#, df) := d := Stack_M(d)
                        kN m
                        A1 := d [1..(rows(d)-1)][1..cols(d)]
                        A2 := stack(fem#, A1)
                        A3 := tot_BMM(A2)^T
                        A4 := stack(df^T, A2, A3)
```

To replace zeros with blank space.  
(To improve readability in Table).

```
format(M#) := for j ∈ [1..rows(M#)]
               for k ∈ [1..cols(M#)]
                 if (M# j k = 0)
                   BB j k := ""
                 else
                   BB j k := M# j k
               BB
```

$P1 := \begin{bmatrix} \text{"Bal"} \\ \text{"CO"} \end{bmatrix}$        $P2 := \begin{bmatrix} \text{"DF"} \\ \text{"FEM"} \end{bmatrix}$

$P3 := \begin{bmatrix} \text{"Final BM"} \end{bmatrix}$

Create Left Stub for Table

```
Create_LS(n) := B := P1
                for j ∈ [1..(n-2)]
                  B := stack(B, P1)
                B := B [1..(rows(B)-1)][1..cols(B)]
                stack(P2, B, P3)
```

## 1. METHOD 1 : Solution : **With Far End Column Moments**

Number of members

$N_{members1} := 16$

PROGRAM : Moment Balancing

```
Bal_M1(M) := dM1 := 0
              dM5 := 0
              dM6 := 0
              dM11 := 0
              dM12 := 0
              dM16 := 0
              dM2 := -M_1 · [D_BA D_BF D_BC]
              dM7 := -(M_2 + M_3) · [D_FE D_FB D_FG D_FK]
              dM13 := -(M_4) · [D_KJ D_KF D_KL]
              A := augment(dM1, dM2, dM5, dM6, dM7)
              A := augment(A, dM11, dM12, dM13, dM16)
```

Moment Carry Over

```
CO_M1(M, BL) := M_1 := 0.5 · BL_2
                 M_3 := 0.5 · BL_8
                 M_5 := 0.5 · BL_4
                 M_6 := 0.5 · BL_7
                 M_8 := 0.5 · BL_3
                 M_10 := 0.5 · BL_14
                 M_11 := 0.5 · BL_9
                 M_12 := 0.5 · BL_13
                 M_14 := 0.5 · BL_10
                 M_16 := 0.5 · BL_15
```

| A  |    | B  |    | C  | E  | F  |    |    |    | G  | J  | K  |    | L  |    |
|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| AB | BA | BF | BC | CB | EF | FE | FB | FG | FK | GF | JK | KJ | KF | KL | LK |

Moment Distribution for METHOD 1  
 iter = Iterations , mem = Number of Elements

```
Find_BMM1 (iter, mem) := "Initialize all row vector"
[ fem_1 mem := 0
  ba_1 mem := 0
  co_1 mem := 0 ]
fem_3 := FEM_BF
fem_8 := - fem_3
fem_10 := FEM_FK
fem_14 := - fem_10
for j ∈ [1..iter]
  if j = 1
    [ fem_3
      fem_8
      fem_10
      fem_14 ]
    ba_j := Bal_M1 [ fem_3
                    fem_8
                    fem_10
                    fem_14 ]
    col_j := CO_M1 (co, ba_j)
  else
    [ co_3
      co_8
      co_10
      co_14 ]
    ba_j := Bal_M1 [ co_3
                    co_8
                    co_10
                    co_14 ]
    col_j := CO_M1 (co, ba_j)
  D_j := stack (ba_j, col_j)
  Arrange (D, fem, DF1)
```

DF for METHOD 1

|        |          |   |      |
|--------|----------|---|------|
| DF1 := | 0        | = |      |
|        | $D_{BA}$ |   | 0    |
|        | $D_{BF}$ |   | 0.32 |
|        | $D_{BC}$ |   | 0.51 |
|        | 0        |   | 0.17 |
|        | 0        |   | 0    |
|        | $D_{FE}$ |   | 0    |
|        | $D_{FB}$ |   | 0.23 |
|        | $D_{FG}$ |   | 0.37 |
|        | $D_{FK}$ |   | 0.12 |
|        | 0        |   | 0.28 |
|        | 0        |   | 0    |
|        | 0        |   | 0    |
|        | $D_{KJ}$ |   | 0.37 |
|        | $D_{KF}$ |   | 0.44 |
|        | $D_{KL}$ |   | 0.19 |
|        | 0        |   | 0    |

LH1 := Create\_LS ( $N_{Iter1} + 1$ )

LH1 =  $\begin{bmatrix} \text{"DF"} \\ \text{"FEM"} \\ \text{"Bal"} \\ \text{"CO"} \\ \text{"Bal"} \\ \text{"CO"} \\ \text{"Bal"} \\ \text{"Final BM"} \end{bmatrix}$

$N_{Iter1} = 3$

$N_{members1} = 16$

rows (LH1) = 8

MD1 := Find\_BMM1 ( $N_{Iter1}$ ,  $N_{members1}$ )

**16 members in Methd 1**

cols (MD1) = 16

MD1 =  $\begin{bmatrix} 0 & 0.32 & 0.51 & 0.17 & 0 & 0 & 0.23 & 0.37 & 0.12 & 0.28 & 0 & 0 & 0.37 & 0.44 \\ 0 & 0 & -181.98 & 0 & 0 & 0 & 0 & 181.98 & 0 & -323.52 & 0 & 0 & 0 & 323.52 \\ 0 & 58.48 & 92.63 & 30.88 & 0 & 0 & 32.92 & 52.14 & 17.38 & 39.1 & 0 & 0 & -119.12 & -141.51 \\ 29.24 & 0 & 26.07 & 0 & 15.44 & 16.46 & 0 & 46.31 & 0 & -70.76 & 8.69 & -59.56 & 0 & 19.55 \\ 0 & -8.38 & -13.27 & -4.42 & 0 & 0 & 5.68 & 9 & 3 & 6.75 & 0 & 0 & -7.2 & -8.55 \\ -4.19 & 0 & 4.5 & 0 & -2.21 & 2.84 & 0 & -6.63 & 0 & -4.28 & 1.5 & -3.6 & 0 & 3.38 \\ 0 & -1.45 & -2.29 & -0.76 & 0 & 0 & 2.54 & 4.02 & 1.34 & 3.01 & 0 & 0 & -1.24 & -1.48 \\ 25.05 & 48.65 & -74.34 & 25.69 & 13.23 & 19.3 & 41.14 & 286.82 & 21.72 & -349.68 & 10.19 & -63.16 & -127.56 & 194.91 \end{bmatrix} \dots$

Format results.  
(replace zeros with blanks)

$C1 := \text{format}(MD1)$

Heading for Results Table

$Hd1 := ["AB" "BA" "BF" "BC" "CB" "EF" "FE" "FB" "FG" "FK" "GF" "JK" "KJ" "KF" "KL" "LK"]$

### METHOD 1 : With Far End Column Moments - 3 Iterations as in Text Book

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|                 | AB    | BA    | BF      | BC    | CB    | EF    | FE    | FB     | FG    | FK      | GF    | JK     | KJ      | KF      | KL     | LK     |
|-----------------|-------|-------|---------|-------|-------|-------|-------|--------|-------|---------|-------|--------|---------|---------|--------|--------|
| <b>DF</b>       |       | 0.32  | 0.51    | 0.17  |       |       | 0.23  | 0.37   | 0.12  | 0.28    |       |        | 0.37    | 0.44    | 0.19   |        |
| <b>FEM</b>      |       |       | -181.98 |       |       |       |       | 181.98 |       | -323.52 |       |        |         | 323.52  |        |        |
| <b>Bal</b>      |       | 58.48 | 92.63   | 30.88 |       |       | 32.92 | 52.14  | 17.38 | 39.1    |       |        | -119.12 | -141.51 | -62.89 |        |
| <b>CO</b>       | 29.24 |       | 26.07   |       | 15.44 | 16.46 |       | 46.31  |       | -70.76  | 8.69  | -59.56 |         | 19.55   |        | -31.45 |
| <b>Bal</b>      |       | -8.38 | -13.27  | -4.42 |       |       | 5.68  | 9      | 3     | 6.75    |       |        | -7.2    | -8.55   | -3.8   |        |
| <b>CO</b>       | -4.19 |       | 4.5     |       | -2.21 | 2.84  |       | -6.63  |       | -4.28   | 1.5   | -3.6   |         | 3.38    |        | -1.9   |
| <b>Bal</b>      |       | -1.45 | -2.29   | -0.76 |       |       | 2.54  | 4.02   | 1.34  | 3.01    |       |        | -1.24   | -1.48   | -0.66  |        |
| <b>Final BM</b> | 25.05 | 48.65 | -74.34  | 25.69 | 13.23 | 19.3  | 41.14 | 286.82 | 21.72 | -349.68 | 10.19 | -63.16 | -127.56 | 194.91  | -67.35 | -33.35 |

C1

$$\text{time}(0) - t_0 = 0.12 \text{ s}$$

| A    | B    |                |      | C    | E    | F    |               |      |                | G    | J     | K      |              |       | L     |
|------|------|----------------|------|------|------|------|---------------|------|----------------|------|-------|--------|--------------|-------|-------|
| AB   | BA   | BF             | BC   | CB   | EF   | FE   | FB            | FG   | FK             | GF   | JK    | KJ     | KF           | KL    | LK    |
|      | 0.32 | 0.51           | 0.17 |      |      | 0.23 | 0.37          | 0.12 | 0.28           |      |       | 0.37   | 0.44         | 0.19  |       |
|      | 58.2 | -181.9<br>92.8 | 30.9 |      |      | 32.5 | 181.9<br>52.3 | 16.9 | -323.2<br>39.6 |      |       | -119.6 | -142.2       | -61.4 |       |
| 29.1 | -8.3 | 26.2<br>-13.4  | -4.5 | 15.5 | 16.3 | 5.7  | 46.4<br>9.1   | 3.0  | -71.1<br>6.9   | 8.5  | -59.8 | -7.3   | 19.8<br>-8.7 | -3.8  | -30.7 |
| -4.2 | -1.5 | 4.6<br>-2.3    | -0.8 | -2.3 | 2.9  | 2.6  | -6.7<br>4.1   | 1.3  | -4.4<br>3.1    | 1.5  | -3.7  | -1.3   | 3.5<br>-1.5  | -0.7  | -1.9  |
| 24.9 | 48.4 | -74.0          | 25.6 | 13.3 | 19.2 | 40.8 | 287.1         | 21.2 | -349.1         | 10.0 | -63.5 | -128.2 | 194.1        | -65.9 | -32.6 |

Fig. 13.6

**Text book results : This gives moments of far end of columns also.**

## 2. METHOD 1 : With More Iterations

$$N_{Iter2} = 6 \quad N_{members1} = 16 \quad LH2 := \text{Create\_LS} (N_{Iter2} + 1)$$

$$MD2 := \text{Find\_BMM1} (N_{Iter2}, N_{members1})$$

$$C2 := \text{format} (MD2)$$

Header same as in Method 1

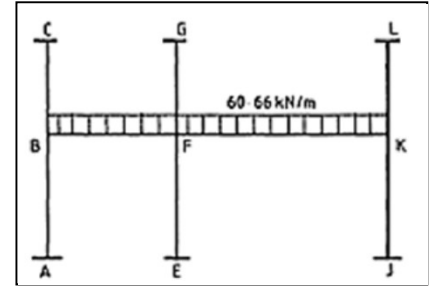
Hd1

Dist Factors same as in Method1

DF1

LH2 =

"DF"  
"FEM"  
"Bal"  
"CO"  
"Bal"  
"CO"  
"Bal"  
"CO"  
"Bal"  
"CO"  
"Bal"  
"CO"  
"Bal"  
"CO"  
"Bal"  
"Final BM"



$$MD2 = \begin{bmatrix} 0 & 0.32 & 0.51 & 0.17 & 0 & 0 & 0.23 & 0.37 & 0.12 & 0.28 & 0 & 0 & 0.37 & 0.44 \\ 0 & 0 & -181.98 & 0 & 0 & 0 & 0 & 181.98 & 0 & -323.52 & 0 & 0 & 0 & 323.52 \\ 0 & 58.48 & 92.63 & 30.88 & 0 & 0 & 32.92 & 52.14 & 17.38 & 39.1 & 0 & 0 & -119.12 & -141.51 \\ 29.24 & 0 & 26.07 & 0 & 15.44 & 16.46 & 0 & 46.31 & 0 & -70.76 & 8.69 & -59.56 & 0 & 19.55 \\ 0 & -8.38 & -13.27 & -4.42 & 0 & 0 & 5.68 & 9 & 3 & 6.75 & 0 & 0 & -7.2 & -8.55 \\ -4.19 & 0 & 4.5 & 0 & -2.21 & 2.84 & 0 & -6.63 & 0 & -4.28 & 1.5 & -3.6 & 0 & 3.38 \\ 0 & -1.45 & -2.29 & -0.76 & 0 & 0 & 2.54 & 4.02 & 1.34 & 3.01 & 0 & 0 & -1.24 & -1.48 \\ -0.72 & 0 & 2.01 & 0 & -0.38 & 1.27 & 0 & -1.15 & 0 & -0.74 & 0.67 & -0.62 & 0 & 1.51 \\ 0 & -0.65 & -1.02 & -0.34 & 0 & 0 & 0.44 & 0.69 & 0.23 & 0.52 & 0 & 0 & -0.55 & -0.66 \\ -0.32 & 0 & 0.35 & 0 & -0.17 & 0.22 & 0 & -0.51 & 0 & -0.33 & 0.12 & -0.28 & 0 & 0.26 \\ 0 & -0.11 & -0.18 & -0.06 & 0 & 0 & 0.2 & 0.31 & 0.1 & 0.23 & 0 & 0 & -0.1 & -0.11 \\ -0.06 & 0 & 0.15 & 0 & -0.03 & 0.1 & 0 & -0.09 & 0 & -0.06 & 0.05 & -0.05 & 0 & 0.12 \\ 0 & -0.05 & -0.08 & -0.03 & 0 & 0 & 0.03 & 0.05 & 0.02 & 0.04 & 0 & 0 & -0.04 & -0.05 \\ 23.95 & 47.85 & -73.11 & 25.26 & 12.64 & 20.89 & 41.81 & 286.13 & 22.07 & -350.01 & 11.03 & -64.1 & -128.25 & 195.97 \end{bmatrix} \dots$$

### METHOD 1 : With Far End Column Moments - With 6 Iterations

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|          | AB    | BA    | BF      | BC    | CB    | EF    | FE    | FB     | FG    | FK      | GF    | JK     | KJ      | KF      | KL     | LK     |
|----------|-------|-------|---------|-------|-------|-------|-------|--------|-------|---------|-------|--------|---------|---------|--------|--------|
| DF       |       | 0.32  | 0.51    | 0.17  |       |       | 0.23  | 0.37   | 0.12  | 0.28    |       |        | 0.37    | 0.44    | 0.19   |        |
| FEM      |       |       | -181.98 |       |       |       |       | 181.98 |       | -323.52 |       |        |         | 323.52  |        |        |
| Bal      |       | 58.48 | 92.63   | 30.88 |       |       | 32.92 | 52.14  | 17.38 | 39.1    |       |        | -119.12 | -141.51 | -62.89 |        |
| CO       | 29.24 |       | 26.07   |       | 15.44 | 16.46 |       | 46.31  |       | -70.76  | 8.69  | -59.56 |         | 19.55   |        | -31.45 |
| Bal      |       | -8.38 | -13.27  | -4.42 |       |       | 5.68  | 9      | 3     | 6.75    |       |        | -7.2    | -8.55   | -3.8   |        |
| CO       | -4.19 |       | 4.5     |       | -2.21 | 2.84  |       | -6.63  |       | -4.28   | 1.5   | -3.6   |         | 3.38    |        | -1.9   |
| Bal      |       | -1.45 | -2.29   | -0.76 |       |       | 2.54  | 4.02   | 1.34  | 3.01    |       |        | -1.24   | -1.48   | -0.66  |        |
| CO       | -0.72 |       | 2.01    |       | -0.38 | 1.27  |       | -1.15  |       | -0.74   | 0.67  | -0.62  |         | 1.51    |        | -0.33  |
| Bal      |       | -0.65 | -1.02   | -0.34 |       |       | 0.44  | 0.69   | 0.23  | 0.52    |       |        | -0.55   | -0.66   | -0.29  |        |
| CO       | -0.32 |       | 0.35    |       | -0.17 | 0.22  |       | -0.51  |       | -0.33   | 0.12  | -0.28  |         | 0.26    |        | -0.15  |
| Bal      |       | -0.11 | -0.18   | -0.06 |       |       | 0.2   | 0.31   | 0.1   | 0.23    |       |        | -0.1    | -0.11   | -0.05  |        |
| CO       | -0.06 |       | 0.15    |       | -0.03 | 0.1   |       | -0.09  |       | -0.06   | 0.05  | -0.05  |         | 0.12    |        | -0.03  |
| Bal      |       | -0.05 | -0.08   | -0.03 |       |       | 0.03  | 0.05   | 0.02  | 0.04    |       |        | -0.04   | -0.05   | -0.02  |        |
| Final BM | 23.95 | 47.85 | -73.11  | 25.26 | 12.64 | 20.89 | 41.81 | 286.13 | 22.07 | -350.01 | 11.03 | -64.1  | -128.25 | 195.97  | -67.72 | -33.85 |

### 3. METHOD 2 : Without Far End Column Moments

DF for METHOD 2

$$DF2 := \begin{matrix} D_{BA} \\ D_{BC} \\ D_{BF} \\ D_{FB} \\ D_{FE} \\ D_{FG} \\ D_{FK} \\ D_{KF} \\ D_{KJ} \\ D_{KL} \end{matrix} = \begin{bmatrix} 0.32 \\ 0.17 \\ 0.51 \\ 0.37 \\ 0.23 \\ 0.12 \\ 0.28 \\ 0.44 \\ 0.37 \\ 0.19 \end{bmatrix}$$

PROGRAM : Moment Balancing

$$\begin{aligned} Bal\_M2(M) &:= \begin{aligned} &dM1 := -M_1 \cdot \begin{bmatrix} D_{BA} & D_{BC} & D_{BF} \end{bmatrix} \\ &dM2 := \left( -\left( M_2 + M_3 \right) \right) \cdot \begin{bmatrix} D_{FB} & D_{FE} & D_{FG} & D_{FK} \end{bmatrix} \\ &dM3 := -M_4 \cdot \begin{bmatrix} D_{KF} & D_{KJ} & D_{KL} \end{bmatrix} \\ &augment(dM1, dM2, dM3) \end{aligned} \end{aligned}$$

Carry Over Moment

$$CO\_M2(M, BL) := \begin{aligned} &M_3 := 0.5 \cdot BL_4 \\ &M_4 := 0.5 \cdot BL_3 \\ &M_7 := 0.5 \cdot BL_8 \\ &M_8 := 0.5 \cdot BL_7 \end{aligned}$$

Moment Distribution for METHOD 2

iter = Iterations , mem = Number of Elements

```
Find_BMM2(iter, mem) := "Initialize all row vector"
    fem_1 mem := 0
    ba_1 mem := 0
    co_1 mem := 0
    fem_3 := FEM_BF
    fem_4 := -fem_3
    fem_7 := FEM_FK
    fem_8 := -fem_7
    for j ∈ [1..iter]
        if j = 1
            fem_3 := fem_3
            fem_4 := fem_4
            fem_7 := fem_7
            fem_8 := fem_8
            ba_j := Bal_M2(fem_3, fem_4, fem_7, fem_8)
            col_j := CO_M2(co, ba_j)
        else
            co_3 := co_3
            co_4 := co_4
            co_7 := co_7
            co_8 := co_8
            ba_j := Bal_M2(co_3, co_4, co_7, co_8)
            col_j := CO_M2(co, ba_j)
        D_j := stack(ba_j, col_j)
    Arrange(D, fem, DF2)
```

$$LH3 := Create\_LS(N_{Iter2} + 1)$$

$$LH3 = \begin{bmatrix} "DF" \\ "FEM" \\ "Bal" \\ "CO" \\ "Bal" \\ "CO" \\ "Bal" \\ "CO" \\ "Bal" \\ "CO" \\ "Bal" \\ "CO" \\ "Bal" \\ "Final BM" \end{bmatrix} \quad \text{rows}(LH3) = 14$$

$$N_{Iter2} = 6$$

$$N_{members1} := 10$$

**10 members in Method 2**

$$MD3 := Find\_BMM2(N_{Iter2}, N_{members1})$$

$$MD3 = \begin{bmatrix} 0.32 & 0.17 & 0.51 & 0.37 & 0.23 & 0.12 & 0.28 & 0.44 & 0.37 & 0.19 \\ 0 & 0 & -181.98 & 181.98 & 0 & 0 & -323.52 & 323.52 & 0 & 0 \\ 58.48 & 30.88 & 92.63 & 52.14 & 32.92 & 17.38 & 39.1 & -141.51 & -119.12 & -62.89 \\ 0 & 0 & 26.07 & 46.31 & 0 & 0 & -70.76 & 19.55 & 0 & 0 \\ -8.38 & -4.42 & -13.27 & 9 & 5.68 & 3 & 6.75 & -8.55 & -7.2 & -3.8 \\ 0 & 0 & 4.5 & -6.63 & 0 & 0 & -4.28 & 3.38 & 0 & 0 \\ -1.45 & -0.76 & -2.29 & 4.02 & 2.54 & 1.34 & 3.01 & -1.48 & -1.24 & -0.66 \\ 0 & 0 & 2.01 & -1.15 & 0 & 0 & -0.74 & 1.51 & 0 & 0 \\ -0.65 & -0.34 & -1.02 & 0.69 & 0.44 & 0.23 & 0.52 & -0.66 & -0.55 & -0.29 \\ 0 & 0 & 0.35 & -0.51 & 0 & 0 & -0.33 & 0.26 & 0 & 0 \\ -0.11 & -0.06 & -0.18 & 0.31 & 0.2 & 0.1 & 0.23 & -0.11 & -0.1 & -0.05 \\ 0 & 0 & 0.15 & -0.09 & 0 & 0 & -0.06 & 0.12 & 0 & 0 \\ -0.05 & -0.03 & -0.08 & 0.05 & 0.03 & 0.02 & 0.04 & -0.05 & -0.04 & -0.02 \\ 47.85 & 25.26 & -73.11 & 286.13 & 41.81 & 22.07 & -350.01 & 195.97 & -128.25 & -67.72 \end{bmatrix}$$

Heading for Results Table

$Hd3 := \text{augment} ("BA", "BC", "BF", "FB", "FE", "FG", "FK", "KF", "KJ", "KL")$

Format results.  
(replace zeros with blanks)

$C3 := \text{format} (MD3)$

| <b>METHOD 2 : Without Far End Column Moments - 6 Iterations</b><br><b>Example 13.1 : Page 398</b><br><b>Reinforced Concrete - Design Theory and Examples</b><br><b>Second Edition - T.J. Macginley &amp; B.S. Choo</b> |       |       |         |        |       |       |         |         |         |        |
|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------|-------|---------|--------|-------|-------|---------|---------|---------|--------|
|                                                                                                                                                                                                                        | BA    | BC    | BF      | FB     | FE    | FG    | FK      | KF      | KJ      | KL     |
| <b>DF</b>                                                                                                                                                                                                              | 0.32  | 0.17  | 0.51    | 0.37   | 0.23  | 0.12  | 0.28    | 0.44    | 0.37    | 0.19   |
| <b>FEM</b>                                                                                                                                                                                                             |       |       | -181.98 | 181.98 |       |       | -323.52 | 323.52  |         |        |
| <b>Bal</b>                                                                                                                                                                                                             | 58.48 | 30.88 | 92.63   | 52.14  | 32.92 | 17.38 | 39.1    | -141.51 | -119.12 | -62.89 |
| <b>CO</b>                                                                                                                                                                                                              |       |       | 26.07   | 46.31  |       |       | -70.76  | 19.55   |         |        |
| <b>Bal</b>                                                                                                                                                                                                             | -8.38 | -4.42 | -13.27  | 9      | 5.68  | 3     | 6.75    | -8.55   | -7.2    | -3.8   |
| <b>CO</b>                                                                                                                                                                                                              |       |       | 4.5     | -6.63  |       |       | -4.28   | 3.38    |         |        |
| <b>Bal</b>                                                                                                                                                                                                             | -1.45 | -0.76 | -2.29   | 4.02   | 2.54  | 1.34  | 3.01    | -1.48   | -1.24   | -0.66  |
| <b>CO</b>                                                                                                                                                                                                              |       |       | 2.01    | -1.15  |       |       | -0.74   | 1.51    |         |        |
| <b>Bal</b>                                                                                                                                                                                                             | -0.65 | -0.34 | -1.02   | 0.69   | 0.44  | 0.23  | 0.52    | -0.66   | -0.55   | -0.29  |
| <b>CO</b>                                                                                                                                                                                                              |       |       | 0.35    | -0.51  |       |       | -0.33   | 0.26    |         |        |
| <b>Bal</b>                                                                                                                                                                                                             | -0.11 | -0.06 | -0.18   | 0.31   | 0.2   | 0.1   | 0.23    | -0.11   | -0.1    | -0.05  |
| <b>CO</b>                                                                                                                                                                                                              |       |       | 0.15    | -0.09  |       |       | -0.06   | 0.12    |         |        |
| <b>Bal</b>                                                                                                                                                                                                             | -0.05 | -0.03 | -0.08   | 0.05   | 0.03  | 0.02  | 0.04    | -0.05   | -0.04   | -0.02  |
| <b>Final BM</b>                                                                                                                                                                                                        | 47.85 | 25.26 | -73.11  | 286.13 | 41.81 | 22.07 | -350.01 | 195.97  | -128.25 | -67.72 |

C3

$\text{time}(0) - t_0 = 0.38 \text{ s}$