

Note: Definitions in "Include Programs.sm" is highlighted in light blue

Includes the definitions from an external SMath file

include("Include_Programs-R10.sm")=43

appVersion(4) = "1.0.8348.30405" appVersion(-4) = "1.0.8348.30405"

Define

kNm := kN m

Assume

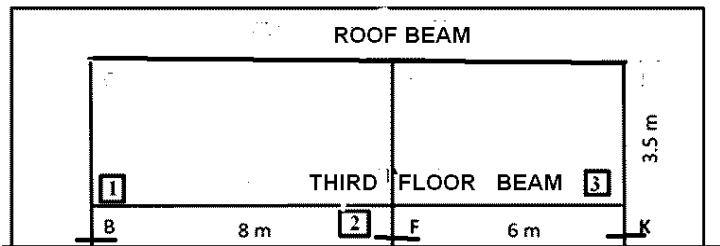
E := 1 MPa

Assume Young's Modulus for RC: This is not really required, but used only for consistent units in intermediate calculations. We can use any numerical value. Ex E = 1 MPa

$t_0 := \text{time}(0)$

Designed and Detailed (BS 8100: 1997) - Page 10 J.B. Higgins and B.R. Rogers (32 pages)

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When considering the **ROOF**, there are no Upper Columns. The **TRICK** is to set sectional dimensions of **Upper Columns (b and h)** equal to zero as **shown below**, But **VECTOR H_{LC}** must have some numerical value. Otherwise, there will be errors due to division by zero. Hence this procedure will make **1** of Upper Columns equal to zero and will give **correct results for Lower Column Moments, Support Moments, Beam Moments and Shear Forces etc.**

All joints on ROOF and 3rd floors are **fixed**. Hence, **FDN** is defined as follows

FDN := 1

DATA: Vectors **b_{uc}** and **h_{uc}** of Upper Cols equal to zero

4 upper columns, 4 lower columns and 3 beams

Column

$b_{uc} := \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \text{ mm}$
 $h_{uc} := \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \text{ mm}$
 $b_{LC} := \begin{bmatrix} 300 \\ 300 \\ 300 \end{bmatrix} \text{ mm}$
 $h_{LC} := \begin{bmatrix} 300 \\ 300 \\ 300 \end{bmatrix} \text{ mm}$
 $H_{uc} := \begin{bmatrix} 3.5 \\ 3.5 \\ 3.5 \end{bmatrix} \text{ m}$
 $H_{LC} := \begin{bmatrix} 3.5 \\ 3.5 \\ 3.5 \end{bmatrix} \text{ m}$

Beam

$b_{beam} := \begin{bmatrix} 300 \\ 300 \end{bmatrix} \text{ mm}$
 $h_{beam} := \begin{bmatrix} 500 \\ 500 \end{bmatrix} \text{ mm}$
 $L := \begin{bmatrix} 8 \\ 6 \end{bmatrix} \text{ m}$

Define

kNm := kN m

Assume

E := 1 MPa

Flanged Beams can be effective only in case of sagging as the concrete is able to take compression. In limit state design we neglect the tensile strength of concrete. As a result, at supports, continuous 'T' beams should be designed as a **rectangular beam (with width equal to the web width)**.

Define

$Line_{zero} := \begin{bmatrix} 0 & 0 \\ \sum \left(\frac{L}{m} \right) & 0 \end{bmatrix}$

Define

$LL [1..rows(L)] := 0 = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$

Moment of Inertia

Upper Columna

$I_{uc} := \frac{1}{12} \cdot b_{uc} \cdot (h_{uc})^3 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \text{ m}^4$

Lower Columna

$I_{LC} := \frac{1}{12} \cdot b_{LC} \cdot (h_{LC})^3 = \begin{bmatrix} 0.0007 \\ 0.0007 \\ 0.0007 \end{bmatrix} \text{ m}^4$

Beams

$I_{beam} := \frac{1}{12} \cdot b_{beam} \cdot (h_{beam})^3 = \begin{bmatrix} 0.0031 \\ 0.0031 \end{bmatrix} \text{ m}^4$

Foundation Columns Fixed at Base

Foundation Columns Fixed at Base

$$FDN = 1$$

Call Program 2 to find the Stiffness Matrix the Substitute Frame

$$K1 := \text{Find_K} \left(L, I_{UC}, I_{LC}, I_{beam}, H_{UC}, H_{LC}, FDN \right) = \begin{bmatrix} 2.3339 & 0.7812 & 0 \\ 0.7812 & 4.4173 & 1.0417 \\ 0 & 1.0417 & 2.8548 \end{bmatrix} \text{ kNm}$$

Frames are spaced at 5 m

$$\begin{aligned} S_{frame} &:= 5 \text{ m} \\ L_{building} &:= 36 \text{ m} \\ \gamma_{cu} &:= 24 \frac{\text{kN}}{\text{m}} \end{aligned} \quad \text{slab}_{thick} := 175 \text{ mm}$$

Loadings

$$\begin{aligned} \text{finishes}_{floor} &:= 1.5 \frac{\text{kN}}{\text{m}^2} \\ q_{k_floor} &:= 1.5 \frac{\text{kN}}{\text{m}^2} \end{aligned}$$

2A. Self weights, Dead loads

Self Weight of Beam

$$W_{beam} := \left(h_{beam} - \text{slab}_{thick} \right) \cdot b_{beam} \cdot \gamma_{cu} = 2.34 \frac{\text{kN}}{\text{m}}$$

D/L from Slab

$$W_{slab} := \text{slab}_{thick} \cdot \gamma_{cu} + \text{finishes}_{floor} = 5.7 \frac{\text{kN}}{\text{m}^2}$$

Floors D/L

$$g_{k_floor} := W_{slab} = 5.7 \frac{\text{kN}}{\text{m}^2}$$

2B. Design Loads on Beams

Dead load

$$G_{k_floor} := g_{k_floor} \cdot S_{frame} + W_{beam} = 30.84 \frac{\text{kN}}{\text{m}}$$

Imposed load

$$Q_{k_floor} := q_{k_floor} \cdot S_{frame} = 7.5 \frac{\text{kN}}{\text{m}}$$

Max Design Load

$$F1 := 1.4 \cdot G_{k_floor} + 1.6 \cdot Q_{k_floor} = 55.18 \frac{\text{kN}}{\text{m}}$$

Min Design Load

$$F2 := 1.0 \cdot G_{k_floor} = 30.84 \frac{\text{kN}}{\text{m}}$$

Define Load Patterns for All 4 Cases

Case I Case II Case III

$$FF := \left[\begin{bmatrix} F1 \\ F1 \end{bmatrix} \begin{bmatrix} F1 \\ F2 \end{bmatrix} \begin{bmatrix} F2 \\ F1 \end{bmatrix} \right] = \left[\begin{bmatrix} 55.18 \\ 55.18 \end{bmatrix} \begin{bmatrix} 55.18 \\ 30.84 \end{bmatrix} \begin{bmatrix} 30.84 \\ 55.18 \end{bmatrix} \right] \frac{\text{kN}}{\text{m}}$$

3 load cases have been considered in this example

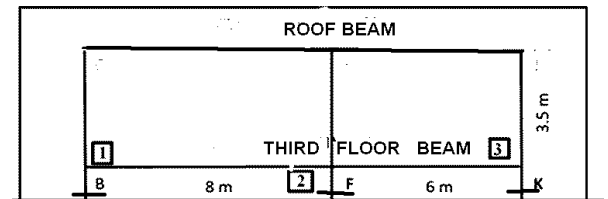
Call Program 7 to find support moments, upper & lower column moments

$$M_{all} := \text{NEW_BMM} \left(FF, K1, H_{UC}, H_{LC}, I_{beam}, I_{UC}, I_{LC}, FDN, L \right)$$

$$FDN = 1$$

$$M_{all} = \begin{bmatrix} \begin{bmatrix} -108.7 & 335.3 \end{bmatrix} & \begin{bmatrix} -301.2 & 32.3 \end{bmatrix} \\ \begin{bmatrix} -115.5 & 300.9 \end{bmatrix} & \begin{bmatrix} -246.5 & 5.1 \end{bmatrix} \\ \begin{bmatrix} -53.9 & 221.7 \end{bmatrix} & \begin{bmatrix} -223 & 45.2 \end{bmatrix} \end{bmatrix} \begin{matrix} \text{Upper} \\ \text{Col} \end{matrix} \begin{matrix} \text{Lower} \\ \text{Col} \end{matrix} \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \begin{bmatrix} 108.7 \\ -34.1 \\ -32.3 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \begin{bmatrix} 115.5 \\ -54.4 \\ -5.1 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \begin{bmatrix} 53.9 \\ 1.3 \\ -45.2 \end{bmatrix} \quad kNm$$

Foundation Columns Fixed at Base



Get Column Moments

$$M_{col} := M_{all} \left[1 \dots \text{rows}(M_{all}) \right] \left[\left(\text{cols}(M_{all}) - 1 \right) \dots \text{cols}(M_{all}) \right]$$

Call Program 9 : Sum of Upper & Lower Col Moments

$$M_{col} = \begin{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \begin{bmatrix} 108.68 \\ -34.09 \\ -32.29 \end{bmatrix} \\ \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \begin{bmatrix} 115.49 \\ -54.45 \\ -5.13 \end{bmatrix} \\ \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \begin{bmatrix} 53.93 \\ 1.31 \\ -45.21 \end{bmatrix} \end{bmatrix} kNm$$

$$Col_Sum := Sum_Col_M(M_{col}) = \begin{bmatrix} \begin{bmatrix} 108.68 \\ 34.09 \\ 32.29 \end{bmatrix} \\ \begin{bmatrix} 115.49 \\ 54.45 \\ 5.13 \end{bmatrix} \\ \begin{bmatrix} 53.93 \\ 1.31 \\ 45.21 \end{bmatrix} \end{bmatrix} kNm$$

Case I

Case II

Case III

Beam1

Center Beam

$$M_{sup} := M_{all} \left[1 \dots \text{rows}(M_{all}) \right] \left[1 \dots \text{rows}(L) \right] = \begin{bmatrix} \begin{bmatrix} -108.7 & 335.3 \end{bmatrix} & \begin{bmatrix} -301.2 & 32.3 \end{bmatrix} \\ \begin{bmatrix} -115.5 & 300.9 \end{bmatrix} & \begin{bmatrix} -246.5 & 5.1 \end{bmatrix} \\ \begin{bmatrix} -53.9 & 221.7 \end{bmatrix} & \begin{bmatrix} -223 & 45.2 \end{bmatrix} \end{bmatrix} kNm$$

Case I

Case II

Case III

Convert the nested matrix to its absolute values

$$MM_{sup} := |M_{sup}| = \begin{bmatrix} \begin{bmatrix} 109 & 335 \end{bmatrix} & \begin{bmatrix} 301 & 32 \end{bmatrix} \\ \begin{bmatrix} 115 & 301 \end{bmatrix} & \begin{bmatrix} 246 & 5 \end{bmatrix} \\ \begin{bmatrix} 54 & 222 \end{bmatrix} & \begin{bmatrix} 223 & 45 \end{bmatrix} \end{bmatrix} kNm$$

SF1
kN

SF2
kN

Max Span M
kNm

X_Max
m

Call PROGRAMS 11 : Find SF, Max Span BM & X_max for ALL Loading Cases

$$Res_All := Find_All (M_{all}, FF, L) = \begin{bmatrix} \begin{bmatrix} 1.92 \cdot 10^5 \frac{kg \cdot m}{s^2} \\ 2.1 \cdot 10^5 \frac{kg \cdot m}{s^2} \end{bmatrix} \begin{bmatrix} -2.49 \cdot 10^5 \frac{kg \cdot m}{s^2} \\ -1.21 \cdot 10^5 \frac{kg \cdot m}{s^2} \end{bmatrix} \begin{bmatrix} -2.27 \cdot 10^5 \frac{kg \cdot m^2}{s^2} \\ -99751.04 \frac{kg \cdot m^2}{s^2} \end{bmatrix} \begin{bmatrix} 3.49 \text{ m} \\ 3.81 \text{ m} \end{bmatrix} \\ \begin{bmatrix} 1.98 \cdot 10^5 \frac{kg \cdot m}{s^2} \\ 1.33 \cdot 10^5 \frac{kg \cdot m}{s^2} \end{bmatrix} \begin{bmatrix} -2.44 \cdot 10^5 \frac{kg \cdot m}{s^2} \\ -52292.42 \frac{kg \cdot m}{s^2} \end{bmatrix} \begin{bmatrix} -2.38 \cdot 10^5 \frac{kg \cdot m^2}{s^2} \\ -39200.31 \frac{kg \cdot m^2}{s^2} \end{bmatrix} \begin{bmatrix} 3.58 \text{ m} \\ 4.3 \text{ m} \end{bmatrix} \\ \begin{bmatrix} 1.02 \cdot 10^5 \frac{kg \cdot m}{s^2} \\ 1.95 \cdot 10^5 \frac{kg \cdot m}{s^2} \end{bmatrix} \begin{bmatrix} -1.44 \cdot 10^5 \frac{kg \cdot m}{s^2} \\ -1.36 \cdot 10^5 \frac{kg \cdot m}{s^2} \end{bmatrix} \begin{bmatrix} -1.16 \cdot 10^5 \frac{kg \cdot m^2}{s^2} \\ -1.22 \cdot 10^5 \frac{kg \cdot m^2}{s^2} \end{bmatrix} \begin{bmatrix} 3.32 \text{ m} \\ 3.54 \text{ m} \end{bmatrix} \end{bmatrix}$$

Case 1
Case 2
Case 3

Note: MATRIX VECTORIZE & TRANSPOSE .Extensively used to transform display of some outputs

CALL PROGRAM 12 : Extract All SFF

$$SFF := Calc_SF (Res_All) = \begin{bmatrix} 192.4 \\ 210.3 \\ 197.5 \\ 132.7 \\ 102.4 \\ 195.2 \end{bmatrix} \begin{bmatrix} -249 \\ -120.7 \\ -243.9 \\ -52.3 \\ -144.3 \\ -135.9 \end{bmatrix} \text{ kN}$$

Convert SFF to absolute values

$$SFF_{ABS} := |SFF| = \begin{bmatrix} 192.4 \\ 210.3 \\ 197.5 \\ 132.7 \\ 102.4 \\ 195.2 \end{bmatrix} \begin{bmatrix} 249 \\ 120.7 \\ 243.9 \\ 52.3 \\ 144.3 \\ 135.9 \end{bmatrix} \text{ kN}$$

Call Program 8

$$SFF_{max} := Find_Max_Abs (SFF_{ABS}) = 249.03 \text{ kN}$$

Beam1

Beam 2

$$\xrightarrow{T} SFF = \begin{bmatrix} L & R \\ 192.4 & -249 \\ 197.5 & -243.9 \\ 102.4 & -144.3 \end{bmatrix} \begin{bmatrix} L & R \\ 210.3 & -120.7 \\ 132.7 & -52.3 \\ 195.2 & -135.9 \end{bmatrix} \text{ kN}$$

CALL PROGRAM 14 : Extract All Span Moments

$$M_{span} := Span_M (Res_All) = \begin{bmatrix} -226.7 \\ -99.8 \\ -238.1 \\ -39.2 \\ -116 \\ -122.1 \end{bmatrix} \text{ kNm}$$

MATRIX VECTORIZE & TRANSPOSE

Beam1

Beam 2

$$\xrightarrow{T} M_{span} = \begin{bmatrix} -226.7 \\ -238.1 \\ -116 \end{bmatrix} \begin{bmatrix} -99.8 \\ -39.2 \\ -122.1 \end{bmatrix} \text{ kNm}$$

CALL PROGRAM 15 : Extract All X-max

$$X_{max} := X_Max (Res_All) = \begin{bmatrix} 3.5 \\ 3.8 \\ 3.6 \\ 4.3 \\ 3.3 \\ 3.5 \end{bmatrix} \text{ m}$$

Case I
Case II
Case III

$$BMD_All := BMD_All_Cases \left(M_{sup}, SFF, L, FF \right)$$

$BMD_All =$	0	108.7		0	301.2		0	115.5		0	246.5		0	53.9	
	0.2	71.3		0.2	260.2		0.2	77.1		0.2	220.6		0.2	34.1	
	0.4	36.1		0.4	221.5		0.4	40.9		0.4	195.9		0.4	15.4	
	0.6	3.2		0.6	184.9		0.6	6.9		0.6	172.4		0.6	-2	
	0.8	-27.6		0.8	150.6		0.8	-24.9		0.8	150.2		0.8	-18.1	
	1	-56.1		1	118.4		1	-54.4		1	129.2		1	-33	
	1.2	-82.5		1.2	88.5		1.2	-81.8		1.2	109.4		1.2	-46.7	
	1.4	-106.6		1.4	60.8		1.4	-107		1.4	90.9		1.4	-59.2	
	1.6	-128.5		1.6	35.3		1.6	-129.9		1.6	73.6		1.6	-70.4	
	1.8	-148.2		1.8	12		1.8	-150.7		1.8	57.5		1.8	-80.4	
	2	-165.7		2	-9.1		2	-169.2		2	42.7		2	-89.2	
	2.2	-181		2.2	-28		2.2	-185.5		2.2	29.1		2.2	-96.7	
	2.4	-194.1		2.4	-44.7		2.4	-199.7		2.4	16.7		2.4	-103	
	2.6	-205		2.6	-59.2		2.6	-211.6		2.6	5.6		2.6	-108	
	2.8	-213.7		2.8	-71.5		2.8	-221.3		2.8	-4.3		2.8	-111.9	
	3	-220.2		3	-81.5		3	-228.8		3	-13		3	-114.4	
	3.2	-224.4		3.2	-89.4		3.2	-234.1		3.2	-20.4		3.2	-115.8	
	3.4	-226.5		3.4	-95.1		3.4	-237.2		3.4	-26.6		3.4	-115.9	
	3.6	-226.3		3.6	-98.5		3.6	-238		3.6	-31.5		3.6	-114.8	
	3.8	-224		3.8	-99.7		3.8	-236.7		3.8	-35.3		3.8	-112.5	
	4	-219.4		4	-98.8		4	-233.2		4	-37.8		4	-108.9	
	4.2	-212.7		4.2	-95.6		4.2	-227.4		4.2	-39		4.2	-104.1	
	4.4	-203.7		4.4	-90.2		4.4	-219.5		4.4	-39.1		4.4	-98	
	4.6	-192.5		4.6	-82.6		4.6	-209.3		4.6	-37.9		4.6	-90.7	
	4.8	-179.1		4.8	-72.8		4.8	-197		4.8	-35.4		4.8	-82.2	
	5	-163.5		5	-60.8		5	-182.4		5	-31.7		5	-72.5	
	5.2	-145.7		5.2	-46.6		5.2	-165.6		5.2	-26.8		5.2	-61.5	
	5.4	-125.7		5.4	-30.2		5.4	-146.7		5.4	-20.7		5.4	-49.3	
	5.6	-103.5		5.6	-11.6		5.6	-125.5		5.6	-13.3		5.6	-35.8	
	5.8	-79.1		5.8	9.3		5.8	-102.1		5.8	-4.7		5.8	-21.2	
	6	-52.4		6	32.3		6	-76.5		6	5.1		6	-5.3	
	6.2	-23.6					6.2	-48.7					6.2	11.9	
	6.4	7.5					6.4	-18.6					6.4	30.3	
	6.6	40.7					6.6	13.6					6.6	49.9	
	6.8	76.2					6.8	48					6.8	70.7	
	7	113.8					7	84.7					7	92.8	
	7.2	153.7					7.2	123.5					7.2	116.1	
	7.4	195.8					7.4	164.5					7.4	140.7	
	7.6	240.1					7.6	207.8					7.6	166.5	
	7.8	286.6					7.8	253.3					7.8	193.5	
	8	335.3					8	300.9					8	221.7	

CALL Program 21 : Coordinates of Max Span Moments

$$Pts_MSpan := Pts_All_Cases \left(X_{max}, M_{span}, L \right) = \begin{bmatrix} \begin{bmatrix} 3.5 & -226.7 \end{bmatrix} \\ \begin{bmatrix} 11.8 & -99.8 \end{bmatrix} \\ \begin{bmatrix} 3.6 & -238.1 \end{bmatrix} \\ \begin{bmatrix} 12.3 & -39.2 \end{bmatrix} \\ \begin{bmatrix} 3.3 & -116 \end{bmatrix} \\ \begin{bmatrix} 11.5 & -122.1 \end{bmatrix} \end{bmatrix}$$

$$X_{max} = \begin{bmatrix} 3.5 \\ 3.8 \\ 3.6 \\ 4.3 \\ 3.3 \\ 3.5 \end{bmatrix} \text{ m} \quad M_{span} = \begin{bmatrix} -226.7 \\ -99.8 \\ -238.1 \\ -39.2 \\ -116 \\ -122.1 \end{bmatrix} \text{ kNm}$$

Call Program 8

$$M_{sup_max} := Find_Max_Abs \left(MM_{sup} \right) = 335.3 \text{ kNm}$$

Use Ceil2 function

$$\left\lceil \frac{M_{sup_max}}{\text{kNm}} \right\rceil_{50} = 350$$

Use Ceil2 function

$$\left\lceil \frac{SFF_{max}}{\text{kN}} \right\rceil_{50} = 250$$

$$MSpan_{ABS} := \left| M_{span} \right|$$

Call Program 8

$$M_Span_{max} := Find_Max_Abs \left(MSpan_{ABS} \right)$$

$$M_Span_{max} = 238.0582 \text{ kNm}$$

CALL Program 23 : X coordinates to plot support moments

$$X_Cord := Sup_Xcord \left(L \right) = \begin{bmatrix} 0 \\ 8 \\ 8 \\ 14 \end{bmatrix} \text{ m}$$

CALL Program 24 : Get BMD Cases

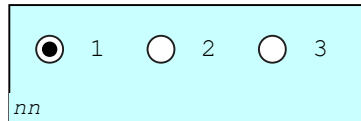
$$BMD := Find_BMD_Cases \left(BMD_All, LL, FF \right)$$

$$\text{rows} \left(BMD \right) = 3$$

$$\text{cols} \left(BMD \right) = 1$$

$$\text{rows} \left(FF_1 \right) = 2$$

$$BM_Case := \left[1 \dots \text{cols} \left(FF \right) \right] = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$$



$$Y_{Sup_Max} := \left\lceil \frac{M_{sup_max}}{\text{kNm}} \right\rceil_{50} = 350$$

$$Y_{Span_Min} := \left\lceil \frac{M_Span_{max}}{\text{kNm}} \right\rceil_{400} = 400$$

Case Number Selected

$$nn = 1$$

$$\frac{M_Span_{max}}{\text{kNm}} = 238.0582$$

X Y Plot Settings

$$PLT := "XYPlot1"$$

$$XYPlot_{XLimMin}_1 := -1$$

$$XYPlot_{XLimMax}_1 := \frac{\sum^L}{m} + 1 = [15]$$

$$XYPlot_{YLimMin}_1 := -Y_{Span_Min} = [-400]$$

$$XYPlot_{YLimMax}_1 := Y_{Sup_Max} = [350]$$

$$XYPlot_{XTick}_1 := 1$$

$$XYPlot_{YTick}_1 := 50$$

$$\text{setprop} \left("XYPlot1.XYLabel.XLabel", "Length \text{ (m)} \right) = 1$$

$$\text{setprop} \left("XYPlot1.XYLabel.YLabel", "BM \text{ (kNm)} \right) = 1$$

```
XY_labelFont (font, pName) := setprop ("{pName}.XYLabel.LabelFont", font)
```

```
XY_labelFont ("Trebuchet MS,8pt", "XYPlot1")=1
```

```
setprop ("XYPlot1.XYLabel.LabelFontColor", "brown")=1
```

nn = 1

```
MyTitle := concat ("ROOF FLOOR BMD: Case ", num2str (nn)) = "ROOF FLOOR BMD: Case 1"
```

```
setprop ("XYPlot1.Title.Text", MyTitle)=1
```

$$Pts_MSpan_{nn} = \begin{bmatrix} 3.5 & -226.7 \\ 11.8 & -99.8 \end{bmatrix}$$

```
setprop ("XYPlot1.Title.TitleFont", "Trebuchet MS,8pt")=1
```

CALL Programs 25 : Plot BMD for a given
CASE Number nn

$$Plot_BMD (nn)^T = \begin{bmatrix} 0 & 108.68 \\ 0.2 & 71.3 \\ 0.4 & 36.14 \\ 0.6 & 3.18 \\ 0.8 & -27.57 \\ 1 & -56.11 \\ 1.2 & -82.45 \\ 1.4 & -106.58 \\ 1.6 & -128.5 \\ 1.8 & -148.22 \\ 2 & -165.73 \\ 2.2 & -181.03 \\ 2.4 & -194.12 \\ 2.6 & -205.01 \\ 2.8 & -213.69 \\ 3 & -220.17 \\ 3.2 & -224.43 \\ 3.4 & -226.49 \\ 3.6 & -226.34 \\ 3.8 & -223.99 \\ 4 & -219.43 \\ 4.2 & -212.66 \\ 4.4 & -203.68 \\ 4.6 & -192.5 \\ 4.8 & -179.11 \\ 5 & -163.51 \\ 5.2 & -145.71 \\ 5.4 & -125.7 \\ 5.6 & -103.48 \\ 5.8 & -79.06 \\ 6 & -52.42 \\ 6.2 & -23.58 \\ 6.4 & 7.46 \\ 6.6 & 40.71 \\ 6.8 & 76.17 \\ 7 & 113.84 \\ 7.2 & 153.72 \\ 7.4 & 195.8 \\ 7.6 & 240.09 \\ 7.8 & 286.58 \\ 8 & 335.28 \end{bmatrix} \begin{bmatrix} 8 & 301.19 \\ 8.2 & 260.23 \\ 8.4 & 221.47 \\ 8.6 & 184.92 \\ 8.8 & 150.57 \\ 9 & 118.44 \\ 9.2 & 88.51 \\ 9.4 & 60.78 \\ 9.6 & 35.27 \\ 9.8 & 11.96 \\ 10 & -9.14 \\ 10.2 & -28.04 \\ 10.4 & -44.73 \\ 10.6 & -59.21 \\ 10.8 & -71.48 \\ 11 & -81.55 \\ 11.2 & -89.41 \\ 11.4 & -95.06 \\ 11.6 & -98.51 \\ 11.8 & -99.75 \\ 12 & -98.78 \\ 12.2 & -95.6 \\ 12.4 & -90.22 \\ 12.6 & -82.63 \\ 12.8 & -72.84 \\ 13 & -60.83 \\ 13.2 & -46.62 \\ 13.4 & -30.2 \\ 13.6 & -11.58 \\ 13.8 & 9.25 \\ 14 & 32.29 \end{bmatrix}$$

CALL Program 27 : Arrange Support Moment
values & X coordinates

$$Pts_MSup := Arrange_M_Sup_All \left(\frac{M_{sup}}{kNm}, \frac{X_Cord}{m} \right) = \begin{bmatrix} 0 & 108.7 \\ 8 & 335.3 \\ 8 & 301.2 \\ 14 & 32.3 \\ 0 & 115.5 \\ 8 & 300.9 \\ 8 & 246.5 \\ 14 & 5.1 \\ 0 & 53.9 \\ 8 & 221.7 \\ 8 & 223 \\ 14 & 45.2 \end{bmatrix}$$

$$M_{sup} = \begin{bmatrix} [-108.7 & 335.3] & [-301.2 & 32.3] \\ [-115.5 & 300.9] & [-246.5 & 5.1] \\ [-53.9 & 221.7] & [-223 & 45.2] \end{bmatrix} kNm$$

$$Pts_MSup_{nn} = \begin{bmatrix} 0 & 108.7 \\ 8 & 335.3 \\ 8 & 301.2 \\ 14 & 32.3 \end{bmatrix} \quad nn = 1$$

CALL Program 28 : Labels to plot

$$Plot_Labs (Pts_MSup_{nn}) = \begin{bmatrix} 0 & 108.7 & "108.7" & 6 & "red" \\ 8 & 335.3 & "335.3" & 6 & "red" \\ 8 & 301.2 & "301.2" & 6 & "red" \\ 14 & 32.3 & "32.3" & 6 & "red" \end{bmatrix}$$

CALL Program 28 : Labels to plot

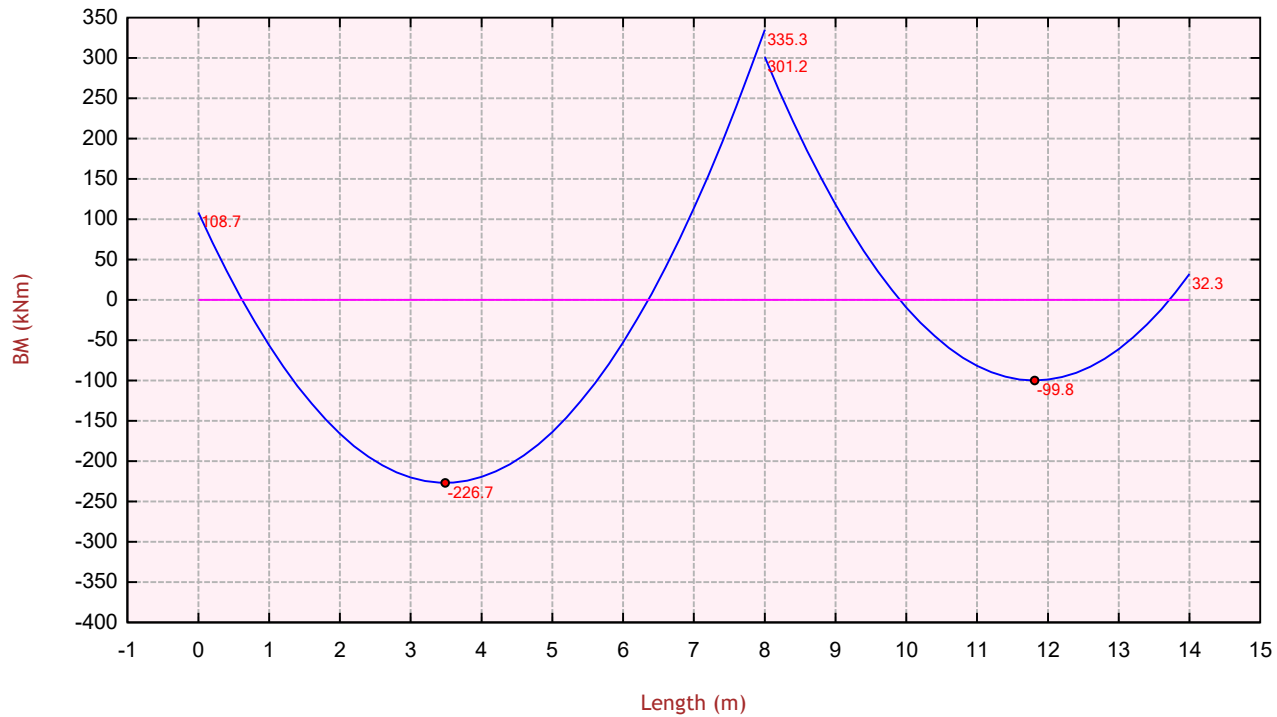
$$Plot_Labs (Pts_MSpan_{nn}) = \begin{bmatrix} 3.5 & -226.7 & "-226.7" & 6 & "red" \\ 11.8 & -99.8 & "-99.8" & 6 & "red" \end{bmatrix}$$

$$Line_{zero} = \begin{bmatrix} 0 & 0 \\ 14 & 0 \end{bmatrix} \quad col \left(MM_{sup}^T, nn \right) = \begin{bmatrix} 109 & 335 \\ 301 & 32 \end{bmatrix} kNm \quad M_{span_{nn}} = \begin{bmatrix} -227 \\ -100 \end{bmatrix} kNm \quad M_{sup_{max}} = 335.3 kNm$$

$$X_{max_{nn}} = \begin{bmatrix} 3.5 \\ 3.8 \end{bmatrix} m \quad FF_{nn} = \begin{bmatrix} 55.176 \\ 55.176 \end{bmatrix} \frac{kN}{m} \quad L = \begin{bmatrix} 8 \\ 6 \end{bmatrix} m$$

$$M_{span_{max}} = 238.1 kNm$$

ROOF FLOOR BMD: Case 1



Results from EXCEL using Stiffness Method

CASE I SUMMARY		Max		Max		
CASE I	68.18			68.18		Case Loading <i>KN/m</i>
-179.62	260.23	402.07	-348.33	119.77	59.66	Beam Moments <i>KNm</i>
108.45			-35.24		-36.02	Upper Column <i>kNm</i>
71.17			-18.50		-23.64	Lower Column <i>kNm</i>
244.90		300.51	252.64		156.42	Shear <i>kN</i>
CASE II SUMMARY		Max		Min		
CASE II	68.18			25.84		Case Loading <i>KN/m</i>
-193.27	276.71	349.74	-250.32	27.88	-4.00	Beam Moments <i>KNm</i>
116.69			-65.19		2.41	Upper Column <i>kNm</i>
76.58			-34.23		1.58	Lower Column <i>kNm</i>
253.15		292.26	119.91		35.13	Shear <i>kN</i>
CASE III SUMMARY		Min		Max		
CASE III	25.84			68.18		Case Loading <i>KN/m</i>
-54.43	83.97	204.72	-230.03	152.85	86.27	Beam Moments <i>KNm</i>
32.87			16.60		-52.09	Upper Column <i>kNm</i>
21.57			8.71		-34.18	Lower Column <i>kNm</i>
84.57		122.15	228.49		180.57	Shear <i>kN</i>

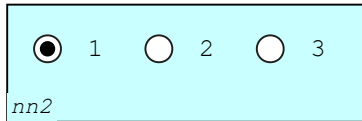
$$time(0) - t_0 = 0.5 \text{ s}$$

Shear Force Diagram

CALL Program 29 : Arrange SF values to PLOT

$$Plot_SF := Arrange_SF(X_Cord, SFF) = \begin{bmatrix} 0 & 192.4 \\ 8 & -249 \\ 8 & 210.3 \\ 14 & -120.7 \\ 0 & 197.5 \\ 8 & -243.9 \\ 8 & 132.7 \\ 14 & -52.3 \\ 0 & 102.4 \\ 8 & -144.3 \\ 8 & 195.2 \\ 14 & -135.9 \end{bmatrix}$$

Define $SF_Case := [1 \dots cols(SF)] = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$



$$nn2 = 1$$

CALL Program 19

$$\frac{Get_L(L)}{m} = \begin{bmatrix} 0 \\ 8 \end{bmatrix}$$

Program 33

$$X_0 = \begin{bmatrix} 0 & 0 \end{bmatrix}$$

CALL Program 31: Labels to print SF zero
x_coordinates on SFD

$$Labs_ZeroSF(n\#) := Find_Labs_ZeroSF(X_{max} \quad n\# \quad 1)$$

$$Labs_ZeroSF(nn2) = \begin{bmatrix} 3.49 & 0 & "3.49" & 6 & "red" \\ 11.81 & 0 & "3.81" & 6 & "red" \end{bmatrix}$$

$$X_L := \text{augment} \left(\sum \left(\frac{L}{m} \right), 0 \right) = \begin{bmatrix} 14 & 0 \end{bmatrix}$$

$$Plot_SF(nn2) := \text{stack}(X_0, Plot_SF_{nn2}, X_L)$$

$$Plot_SF(nn2) = \begin{bmatrix} 0 & 0 \\ 0 & 192.4 \\ 8 & -249 \\ 8 & 210.3 \\ 14 & -120.7 \\ 14 & 0 \end{bmatrix}$$

CALL Program 30 :Labels to print SF values on SFD

$$Plot_Labs_SF(Plot_SF_{nn2}) = \begin{bmatrix} 0 & 192.38 & "192.4" & 6 & "black" \\ 8 & -249.03 & "-249.0" & 6 & "black" \\ 8 & 210.35 & "210.4" & 6 & "black" \\ 14 & -120.71 & "-120.7" & 6 & "black" \end{bmatrix}$$

X Y Plot Settings for SFD

$$XYPlot_{XLimMin}_2 := -1 \quad XYPlot_{XLimMax}_2 := \frac{\sum L}{m} + 2 = \begin{bmatrix} 15 \\ 16 \end{bmatrix} \quad Y_{SF_Max} := \left\lfloor \frac{SFF_{max}}{kN} \right\rfloor_{20} = 260$$

$$XYPlot_{YLimMin}_2 := -Y_{SF_Max} - 50 \quad XYPlot_{YLimMax}_2 := Y_{SF_Max}$$

$$XYPlot_{XTick}_2 := 1 \quad XYPlot_{YTick}_2 := 50 \quad LL = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$setprop("XYPlot2.XYLabel.XLabel", "Length (m)") = 1$$

$$setprop("XYPlot2.XYLabel.YLabel", "SF (kN)") = 1$$

$$XY_{labelFont}(font, pName) := setprop("{pName}.XYLabel.LabelFont", font)$$

$$XY_{labelFont}("Trebuchet MS, 8pt", "XYPlot2") = 1$$

$$setprop("XYPlot2.XYLabel.LabelFontColor", "brown") = 1$$

$$MyTitle := concat("ROOF FLOOR SFD: Case ", num2str(nn2)) = "ROOF FLOOR SFD: Case 1"$$

$$setprop("XYPlot2.Title.Text", MyTitle) = 1$$

$$setprop("XYPlot2.Title.TitleFont", "Trebuchet MS, 8pt") = 1 \quad SFF_{max} = 249 \text{ kN}$$

$$Zero_{SF}(nn2) := augment\left(\frac{Get_L(L) + X_{max} nn2}{m}, LL\right) = \begin{bmatrix} 3.49 & 0 \\ 11.81 & 0 \end{bmatrix} \quad Get_L(L) = \begin{bmatrix} 0 \\ 8 \end{bmatrix} m \quad X_{max} nn2 = \begin{bmatrix} 3.49 \\ 3.81 \end{bmatrix} m \quad LL = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$Labs_ZeroSF(nn2) = \begin{bmatrix} 3.49 & 0 & "3.49" & 6 & "red" \\ 11.81 & 0 & "3.81" & 6 & "red" \end{bmatrix}$$

$$Plot_Labs_SF(Plot_SF_{nn2}) = \begin{bmatrix} 0 & 192.4 & "192.4" & 6 & "black" \\ 8 & -249 & "-249.0" & 6 & "black" \\ 8 & 210.3 & "210.4" & 6 & "black" \\ 14 & -120.7 & "-120.7" & 6 & "black" \end{bmatrix} \quad Plot_SF(nn2) = \begin{bmatrix} 0 & 0 \\ 0 & 192.38 \\ 8 & -249.03 \\ 8 & 210.35 \\ 14 & -120.71 \\ 14 & 0 \end{bmatrix}$$

Results from EXCEL using Stiffness Method

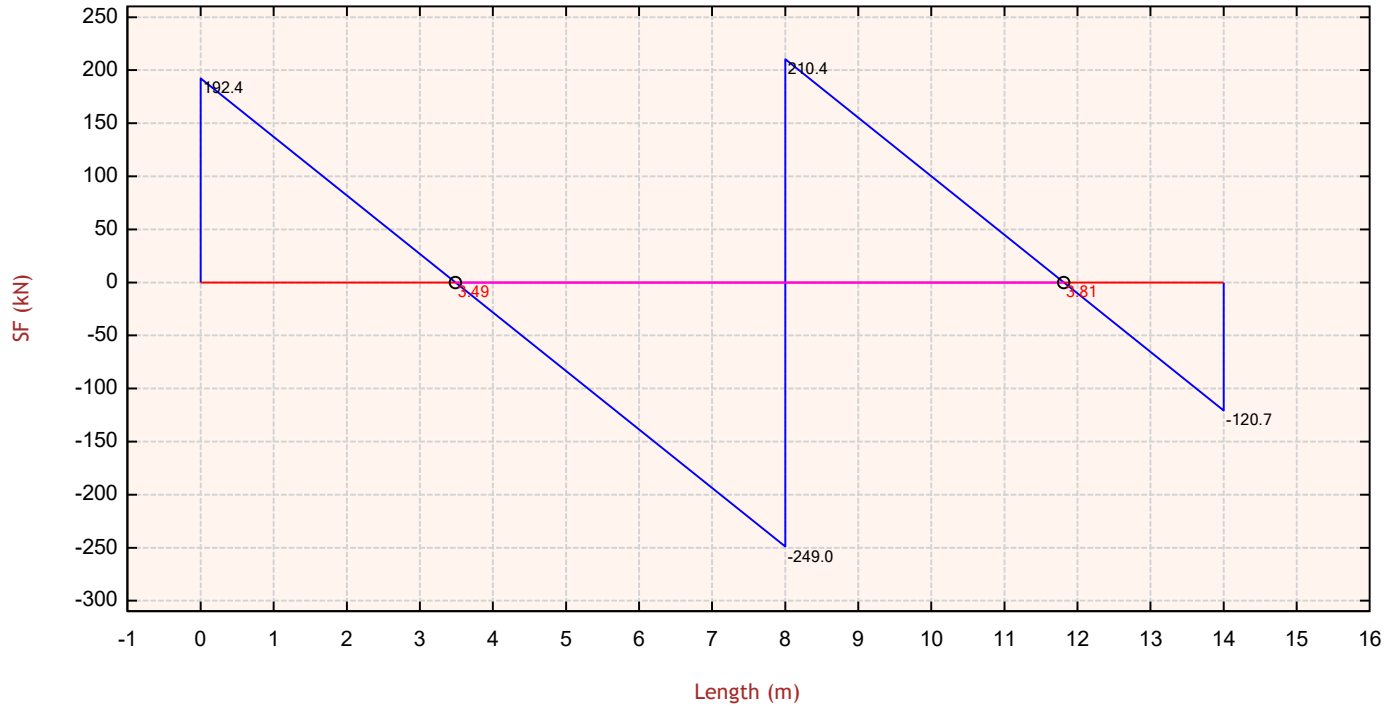
CASE I SUMMARY				Max				
CASE I	68.18			68.18		Case Loading <i>KN/m</i>		
-179.62	260.23	402.07	-348.33	119.77	59.66	Beam Moments <i>KNm</i>		
108.45			-35.24		-36.02	Upper Column <i>kNm</i>		
71.17			-18.50		-23.64	Lower Column <i>kNm</i>		
244.90		300.51	252.64		156.42	Shear <i>kN</i>		
CASE II SUMMARY				Min				
CASE II	68.18			25.84		Case Loading <i>KN/m</i>		
-193.27	276.71	349.74	-250.32	27.88	-4.00	Beam Moments <i>KNm</i>		
116.69			-65.19		2.41	Upper Column <i>kNm</i>		
76.58			-34.23		1.58	Lower Column <i>kNm</i>		
253.15		292.26	119.91		35.13	Shear <i>kN</i>		
CASE III SUMMARY				Max				
CASE III	25.84			68.18		Case Loading <i>KN/m</i>		
-54.43	83.97	204.72	-230.03	152.85	86.27	Beam Moments <i>KNm</i>		
32.87			16.60		-52.09	Upper Column <i>kNm</i>		
21.57			8.71		-34.18	Lower Column <i>kNm</i>		
84.57		122.15	228.49		180.57	Shear <i>kN</i>		

Beam Shear Forces

$$\overrightarrow{SFF}^T = \begin{bmatrix} \text{Beam 1} & \text{Beam 2} \\ \text{L} & \text{R} & \text{L} & \text{R} \end{bmatrix} = \begin{bmatrix} \begin{bmatrix} 192 & -249 \\ 198 & -244 \\ 102 & -144 \end{bmatrix} & \begin{bmatrix} 210 & -121 \\ 133 & -52 \\ 195 & -136 \end{bmatrix} \end{bmatrix} \text{ kN}$$

Case 1
Case 2
Case 3

ROOF FLOOR SFD: Case 1



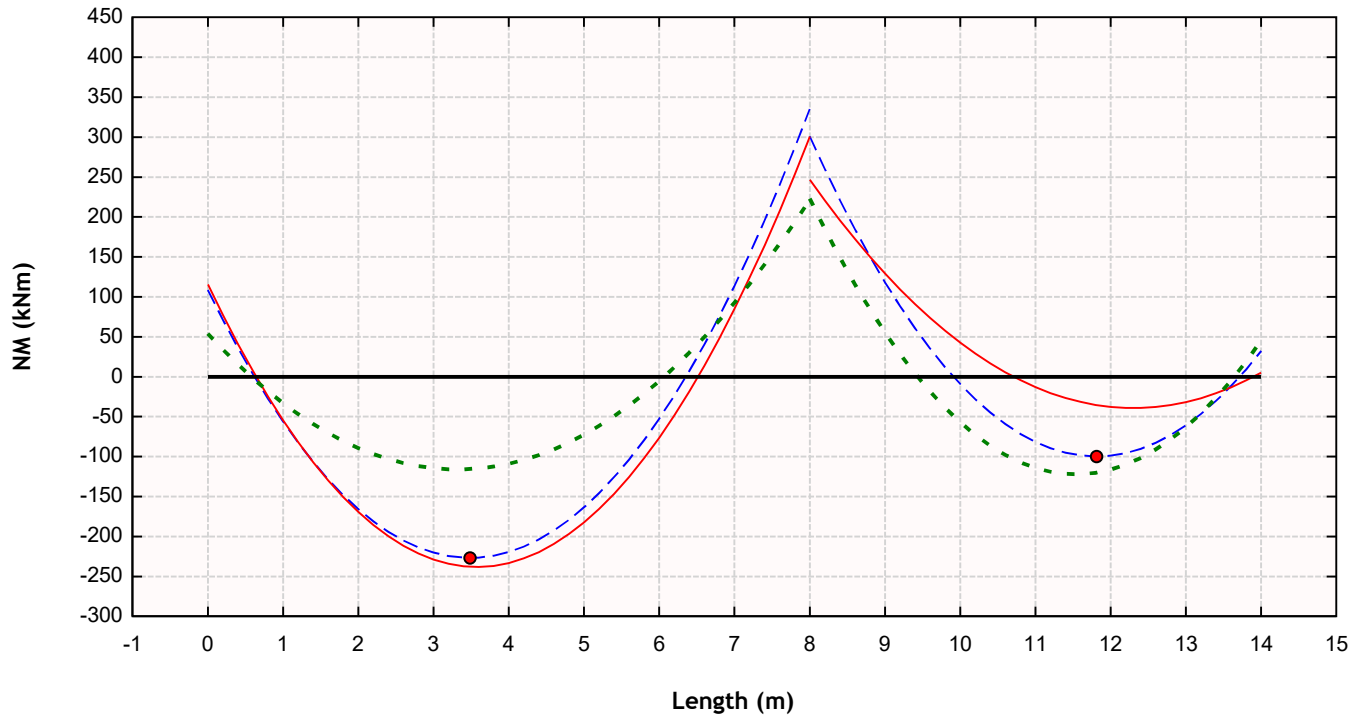
INTERNAL COLUMN (Foundation → Roof) AXIAL LOADING and MOMENTS from ANALYSIS

LOAD CASE	BEAM LOADS kN		COLUMN DESIGN LOADS kN				COL. MOMENTS kNm			
	TOTAL		IMPOSED		DEAD		TOP		BOTTOM	
	1	2	1	2	1	2	1	2	1	2
Roof	249	244	54	53	195	191	34	54		
SW	210	133	46		164	133			32	58
					9	9				
3rd Fl.	298	290	140	136	158	154	32	58		
SW	249	117	117		132	117			32	58
					9	9				
2nd Fl.	298	290	140	136	158	154	32	58		
SW	249	117	117		132	117			35	65
					9	9				
1st Fl.	300	292	141	137	159	155	19	34		
SW	252	120	118		134	120			-	-
					14	14				
Fnds.			873	462	1273	1182				

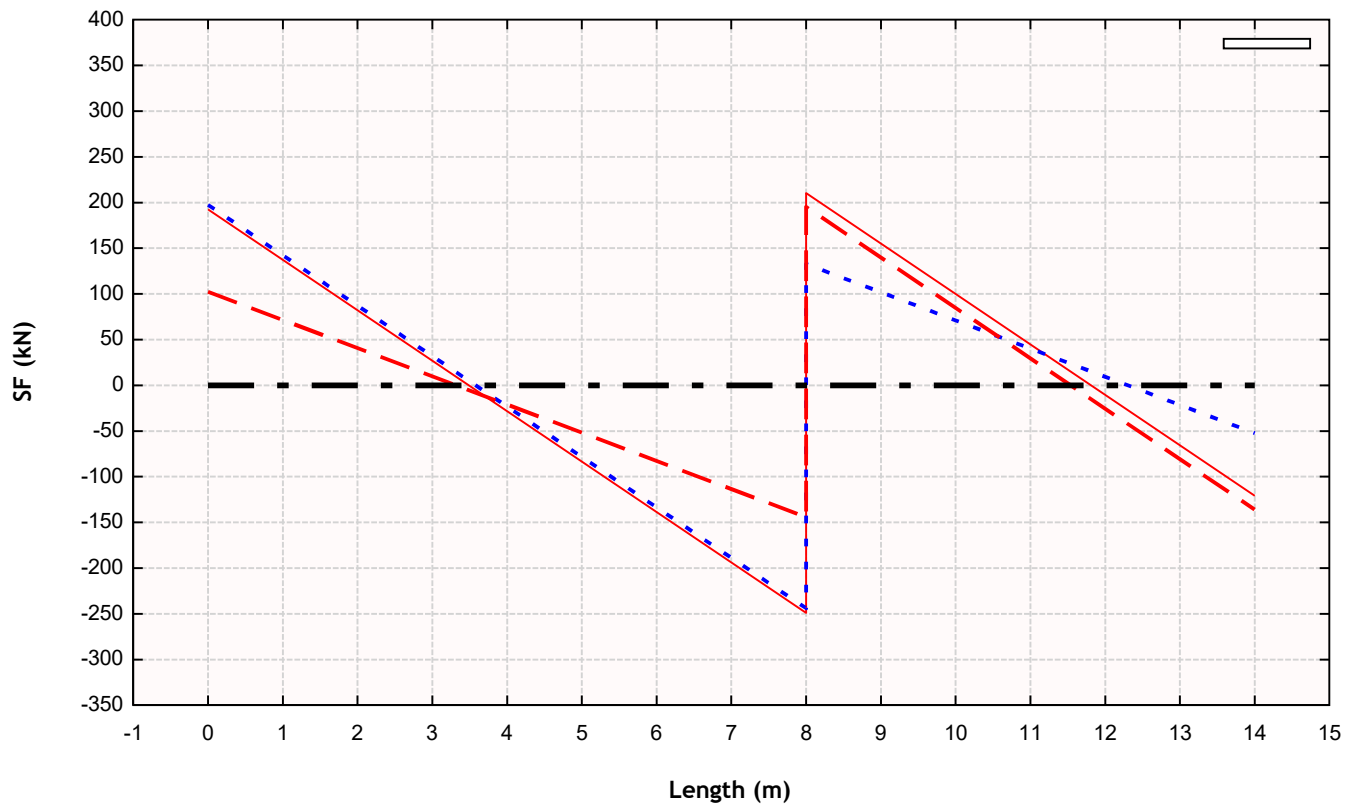
Internal Columns

$$\overrightarrow{SFF}^T = \begin{bmatrix} \begin{bmatrix} 192 & -249 \\ 198 & -244 \\ 102 & -144 \end{bmatrix} & \begin{bmatrix} 210 & -121 \\ 133 & -52 \\ 195 & -136 \end{bmatrix} \end{bmatrix} \text{ kN}$$

ROOF BMD All Cases



ROOF SFD All Cases



time (0) - $t_0 = 0.7$ s

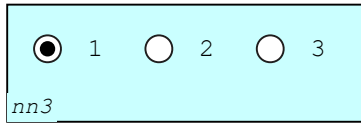
Plotting Column Moments

Unlike BMD and SFD, plotting Column Moments is relatively difficult. The main reason is that both Column Moments and the Column locations have to be plotted on the X-axis. Hence, Column moment values are divided by total length of the horizontal beams. Then these values are converted to strings and plotted at the proper locations for both upper and lower columns.

$$M_{col} = \begin{matrix} \text{Upper} & \text{Lower} \\ \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} & \begin{bmatrix} 108.7 \\ -34.1 \\ -32.3 \end{bmatrix} \\ \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} & \begin{bmatrix} 115.5 \\ -54.4 \\ -5.1 \end{bmatrix} \\ \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} & \begin{bmatrix} 53.9 \\ 1.3 \\ -45.2 \end{bmatrix} \end{matrix} \text{ kNm}$$

Define $Col_Case := [1 \dots cols(F)] = \begin{bmatrix} 1 \\ 2 \\ 3 \end{bmatrix}$

Number of Columns
 $N_{cols} := rows(L) + 1 = 3$



$$nn3 = 1$$

$$Max_{col_top} := Max(Max_Abs(col(M_{col}, 1))) = 0 \text{ kNm}$$

$$Min_{col_top} := Min(Min_Abs(col(M_{col}, 1))) = 0 \text{ kNm}$$

$$Max_{col_bot} := Max(Max_Abs(col(M_{col}, 2))) = 115.5 \text{ kNm}$$

$$Min_{col_bot} := Min(Min_Abs(col(M_{col}, 2))) = 1.3 \text{ kNm}$$

Scale to plot column moments

$$SC := round\left(\frac{Max_{col_top}}{Max_{col_bot}}, 1\right) = 0$$



Note: In **CASES 1 & 2**, the column moments at joint 1 are large compared to CASE 3. Hence, the plot will look odd, and to avoid such a situation, a **SCALE** is arbitrarily introduced in PLOTTING the column moments

However, above value of **SC** is too small, and will distort the PLOT. Hence, change it with **trial and error**.

$$SC := 1.5$$

$$nn3 = 1 \quad FDN = 1 \quad \text{Already defined at the start}$$

Call Program 36: To Plot Upper Column Moments

$$MCol_{top} := Plot_UP_Col_M(col(M_{col}, 1), L, nn3, H_{UC}, 1, SC)$$

Call Program 37: To Plot Lower Column Moments

$$MCol_{bot} := Plot_LOW_Col_M(col(M_{col}, 2), L, nn3, H_{LC}, -1, FDN, SC)$$

CALL Program 38: Convert Top Col Moments to strings

$$MSTR_{top} := MStr2_{top}(nn3, M_{col}) = \begin{bmatrix} "0" \\ "0" \\ "0" \end{bmatrix}$$

CALL Program 38: Convert Bot Col Moments to strings

$$MSTR_{bot} := MStr2_{bot}(nn3, M_{col}) = \begin{bmatrix} "109" \\ "-34" \\ "-32" \end{bmatrix}$$

Call Program 35: Stack Upper Col matrices

$$Cords_{top} := STACK \left(MCol_{top} \begin{bmatrix} 1 \dots N_{cols} \end{bmatrix} \right) = \begin{bmatrix} 0 & 0 \\ 8 & 0 \\ 14 & 0 \end{bmatrix}$$

Call Program 35: Stack Bottom Col matrices

$$Cords_{bot} := STACK \left(MCol_{bot} \begin{bmatrix} 1 \dots (N_{cols}) \end{bmatrix} \right) = \begin{bmatrix} -5.2 & 0 \\ 9.6 & 0 \\ 15.5 & 0 \end{bmatrix}$$

Upper Column - Cordinates to plot moments

$$MCol_{top} = \begin{bmatrix} \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix} \\ \begin{bmatrix} 8 & 0 \\ 8 & 0 \end{bmatrix} \\ \begin{bmatrix} 14 & 0 \\ 14 & 0 \end{bmatrix} \\ \begin{bmatrix} 0 & 0 \\ 0 & 3.5 \end{bmatrix} \\ \begin{bmatrix} 8 & 0 \\ 8 & 3.5 \end{bmatrix} \\ \begin{bmatrix} 14 & 0 \\ 14 & 3.5 \end{bmatrix} \\ \begin{bmatrix} 0 & 3.5 \\ 0 & 3.5 \end{bmatrix} \\ \begin{bmatrix} 8 & 3.5 \\ 8 & 3.5 \end{bmatrix} \\ \begin{bmatrix} 14 & 3.5 \\ 14 & 3.5 \end{bmatrix} \\ \begin{bmatrix} 0 & 3.5 \\ 0 & 0 \end{bmatrix} \\ \begin{bmatrix} 8 & 3.5 \\ 8 & 0 \end{bmatrix} \\ \begin{bmatrix} 14 & 3.5 \\ 14 & 0 \end{bmatrix} \end{bmatrix}$$

Upper column

Upper Vertical lines

Far end of upper column.

Bottom Column - Cordinates to plot moments

$$MCol_{bot} = \begin{bmatrix} \begin{bmatrix} 0 & 0 \\ -5.2 & 0 \end{bmatrix} \\ \begin{bmatrix} 8 & 0 \\ 9.6 & 0 \end{bmatrix} \\ \begin{bmatrix} 14 & 0 \\ 15.5 & 0 \end{bmatrix} \\ \begin{bmatrix} 0 & 0 \\ 0 & -3.5 \end{bmatrix} \\ \begin{bmatrix} 8 & 0 \\ 8 & -3.5 \end{bmatrix} \\ \begin{bmatrix} 14 & 0 \\ 14 & -3.5 \end{bmatrix} \\ \begin{bmatrix} 2.6 & -3.5 \\ 0 & -3.5 \end{bmatrix} \\ \begin{bmatrix} 7.2 & -3.5 \\ 8 & -3.5 \end{bmatrix} \\ \begin{bmatrix} 13.2 & -3.5 \\ 14 & -3.5 \end{bmatrix} \\ \begin{bmatrix} 2.6 & -3.5 \\ -5.2 & 0 \end{bmatrix} \\ \begin{bmatrix} 7.2 & -3.5 \\ 9.6 & 0 \end{bmatrix} \\ \begin{bmatrix} 13.2 & -3.5 \\ 15.5 & 0 \end{bmatrix} \end{bmatrix}$$

Bottom column

Bottom Vertical lines

Far end of bottom column.

Call Program 40: Plot UPPER column moment string values

$$PTS_{top} := Plot_Pts \left(nn3, Cords_{top}, MSTR_{top} \right)$$

Call Program 40: Plot BOTTOM column moment string values

$$PTS_{bot} := Plot_Pts \left(nn3, Cords_{bot}, MSTR_{bot} \right)$$

$$PTS_{top} = \begin{bmatrix} 0 & 0 & "0" & 6 & "black" \\ 8 & 0 & "0" & 6 & "black" \\ 14 & 0 & "0" & 6 & "black" \end{bmatrix}$$

$$PTS_{bot} = \begin{bmatrix} -5.2 & 0 & "109" & 6 & "black" \\ 9.6 & 0 & "-34" & 6 & "black" \\ 15.5 & 0 & "-32" & 6 & "black" \end{bmatrix} \quad \begin{array}{l} FDN = 1 \\ nn3 = 1 \end{array}$$

XY Plot Settings for Column Moment Diagram

CASE $nn3 = 1$

$$XYPlot_{XLimMin}_5 := -6 \quad XYPlot_{XLimMax}_5 := \frac{\sum^L m}{m} + 4 \quad Y_{Col_Max} := \frac{\text{Max} \left(H_{LC}, H_{UC} \right)}{m} + 1 = 4.5$$

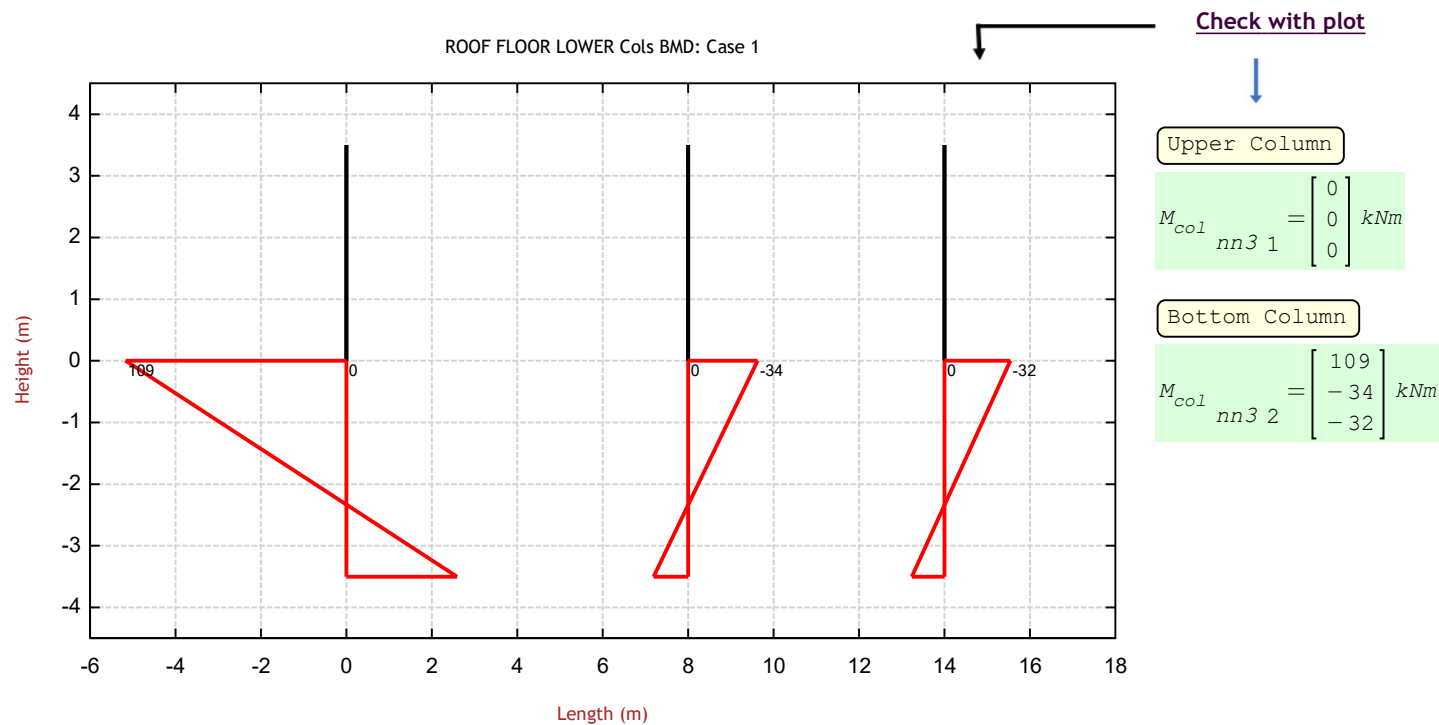
$$XYPlot_{YLimMin}_5 := -Y_{Col_Max} \quad XYPlot_{YLimMax}_5 := Y_{Col_Max}$$

$$XYPlot_{XTick}_5 := 2 \quad XYPlot_{YTick}_5 := 1$$

$$FDN_{cond} := \left| \begin{array}{l} TXT := \begin{cases} "Fixed Foundation" & \text{if } FDN = 1 \\ "Pinned Foundation" & \text{otherwise} \end{cases} \end{array} \right|$$

```
setprop("XYPlot5.XYLabel.XLabel", "Length (m)")=1
setprop("XYPlot5.XYLabel.YLabel", "Height (m)")=1
XY_labelFont(font, pName):=setprop("{pName}.XYLabel.LabelFont", font)
XY_labelFont("Trebuchet MS, 7pt", "XYPlot5")=1
setprop("XYPlot5.XYLabel.LabelFontColor", "brown")=1
MyTitle:=concat("ROOF FLOOR LOWER Cols BMD: Case ", num2str(nn3))="ROOF FLOOR LOWER Cols BMD: Case 1"
setprop("XYPlot5.Title.Text", MyTitle)=1
setprop("XYPlot5.Title.TitleFont", "Trebuchet MS, 7pt")=1
```

Case number nn3 = 1 FDN = 1 Foundation Columns Fixed at Base



Upper Column	Bottom Column	time (0) - t ₀ = 0.7 s	
$M_{col \quad 1 \quad 1} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \text{ kNm}$	$M_{col \quad 1 \quad 2} = \begin{bmatrix} 109 \\ -34 \\ -32 \end{bmatrix} \text{ kNm}$		Case 1
Upper Column	Bottom Column		
$M_{col \quad 2 \quad 1} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \text{ kNm}$	$M_{col \quad 2 \quad 2} = \begin{bmatrix} 115 \\ -54 \\ -5 \end{bmatrix} \text{ kNm}$	Case 2	
Upper Column	Bottom Column	Case 3	
$M_{col \quad 3 \quad 1} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \text{ kNm}$	$M_{col \quad 3 \quad 2} = \begin{bmatrix} 54 \\ 1 \\ -45 \end{bmatrix} \text{ kNm}$		