

## Linkage bars animations

Linkage Bars

Examples

$$\text{Clear}(N, t, \tau, x, y, z, \theta, \omega) = 1$$

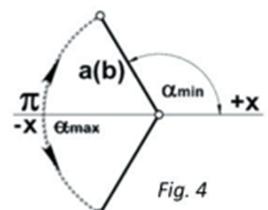
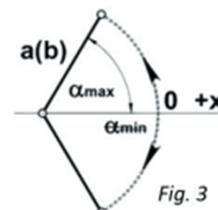
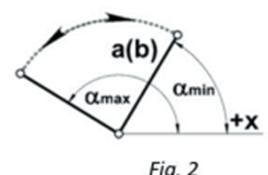
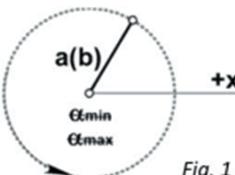
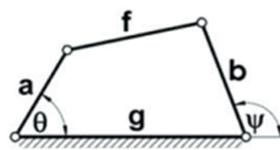
4-bar

### Four Bar Mechanism

Reference

[https://www.researchgate.net/publication/325172892\\_Classification\\_geometrical\\_and\\_kinematic\\_analysis\\_of\\_four-bar\\_linkages/link/5bce3cdc299bf1a43d9a38ff/download](https://www.researchgate.net/publication/325172892_Classification_geometrical_and_kinematic_analysis_of_four-bar_linkages/link/5bce3cdc299bf1a43d9a38ff/download)

There are  $3^3 = 27$  different configuration types considering movement performed by input link a and output link b. If a link performs a complete rotation it is called a crank and a rocker if not, with both limits  $\alpha_{\min}$  and  $\alpha_{\max}$  for the angle.



The case 0-rocker is when not exist  $\alpha_{\min}$  and the link oscillates about 0 with amplitude  $\pm \alpha_{\max}$ .

The case  $\pi$ -rocker is when not exist  $\alpha_{\max}$  and the link oscillates about  $\pi$  with amplitude  $\pi \pm \alpha_{\max}$ .

$\text{Bar4}(a, b, f, g)$  returns the classification and the angles.

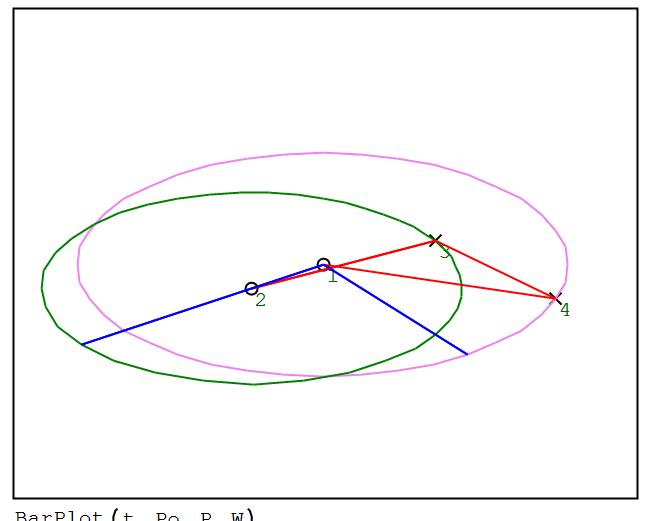
### Double crank

- In this example N + 1 is the numbers of frames in the animation, n the variable for it,
- The two first rows in E are the node numbers and the third the lenght for each bar.
- Po are the x,y,z coordinates of the fixes nodes and Pg the guess values for the coordinates of the movable nodes.
- $\theta_0$  is a vector with N + 1 values for the rotating angle.

```

[ N := 40 n := [1..(N+1)] θ₀ := pR(0 °, 360 °, N) ]
[ a := 1.4 b := 1.2 f := 1 g := 0.5 ]
[ Po := [0 0 0] Pg := [0 b 0] ]
[ Po := [g 0 0] Pg := [f b 0] ]
E := [ 2 3 4
      3 4 1
      b f a ]
      BarR(θ₀, x₄, y₄)
BarE(θ₀, x, y, z) := [ BarR(θ₀, x₄, y₄)
                        z₃
                        z₄ ]
[ P W ] := BarPW(θ₀, E, Po, Pg)

```



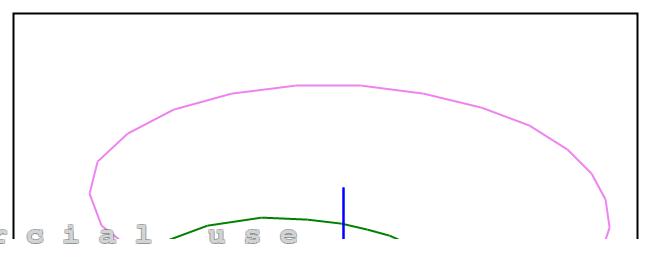
$$\text{Bar4}(a, b, f, g) = \begin{bmatrix} \text{"Inp link a"} & \text{"θmin"} & \text{"θmax"} & \text{"Out link b"} & \text{"ψmin"} & \text{"ψmax"} \\ \text{"crank"} & \text{"E"} & \text{"E"} & \text{"crank"} & \text{"E"} & \text{"E"} \end{bmatrix}$$

We can change the speed of  $\theta_0$  adding a mapping expression in pR. Also can change the z-values, by fixed values or using  $\tau$ , ranged between 0 and 1

```

[ N := 40 n := [1..(N+1)] θ₀ := pR(0, 2·π, N, x²) ]
[ a := 1.4 b := 1 f := 1.2 g := 0.4 zo := 0.5 ]
[ Po := [0 0 0] Pg := [g -b 0] ]
[ Po := [g 0 -zo] Pg := [a 0 0] ]
[ 2 3 4 ] . Note for commercial use

```



12 mar. 2023 05:29:33 - F:\USERS\Desktop\LinkageBars.pdf

```

Create[3 4 1] usd:= $\frac{\tau}{N}$ 
BarE ( $\theta, x, y, z$ ) :=  $\begin{bmatrix} BarR (\theta, x_4, y_4) \\ z_3 \\ z_4 - zo \cdot \tau \end{bmatrix}$ 
[ P W ] := BarPW ( $\theta_o, E, Po, Pg$ )

```

BarPlot (t, Po, P, W)

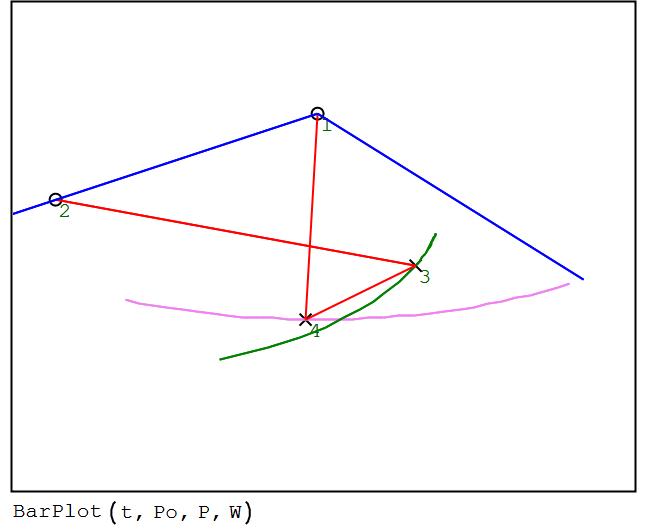
### Double rocker

In this example we use Bar4 for get the angle bounds and construct  $\theta_o$  for the forward and retrun paths.

```

N := 60 n := [1..(N+1)]  $\theta_o := pR (29^\circ, 88^\circ, 0.5 \cdot N)$ 
 $\theta_o := eval (stack (\theta_o, reverse (\theta_o)))$ 
[ a := 1.4 b := 1.2 f := 0.5 g := 1 ]
[ Po := [ 0 0 0 ] Pg := [ 0 b 0 ] ]
E := [ 2 3 4 ]
[ 3 4 1 ]
[ b f a ]
BarE ( $\theta, x, y, z$ ) :=  $\begin{bmatrix} BarR (\theta, x_4, y_4) \\ z_3 \\ z_4 \end{bmatrix}$ 
[ P W ] := BarPW ( $\theta_o, E, Po, Pg$ )

```



$$Bar4 (a, b, f, g) = \begin{bmatrix} "Inp link a" "θmin" "θmax" "Out link b" "ψmin" "ψmax" \\ "rocker" 28.0981 88.5675 "rocker" 60.8236 132.7786 \end{bmatrix}$$

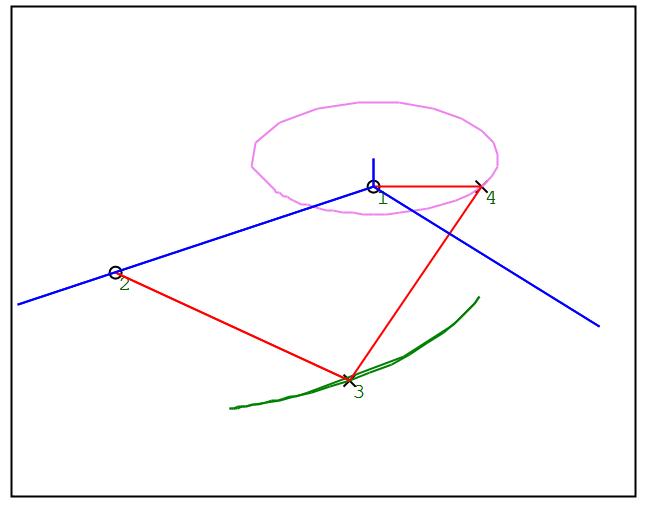
### Crank - rocker

We add an small zo, which not change the mechanism type, and the angles  $\psi$

```

N := 40 n := [1..(N+1)]
 $\theta_o := pR (0, 2 \cdot \pi, N, e^{3 \cdot x} - 1)$ 
[ a := 0.4 b := 1.2 f := 1.4 g := 1 zo := 0.1 ]
[ Po := [ 0 0 0 ] Pg := [ g b zo ] ]
E := [ 2 3 4 ]
[ 3 4 1 ]
[ b f a ]
BarE ( $\theta, x, y, z$ ) :=  $\begin{bmatrix} BarR (\theta, x_4, y_4) \\ z_3 - zo \\ z_4 - zo \end{bmatrix}$ 
[ P W ] := BarPW ( $\theta_o, E, Po, Pg$ )

```

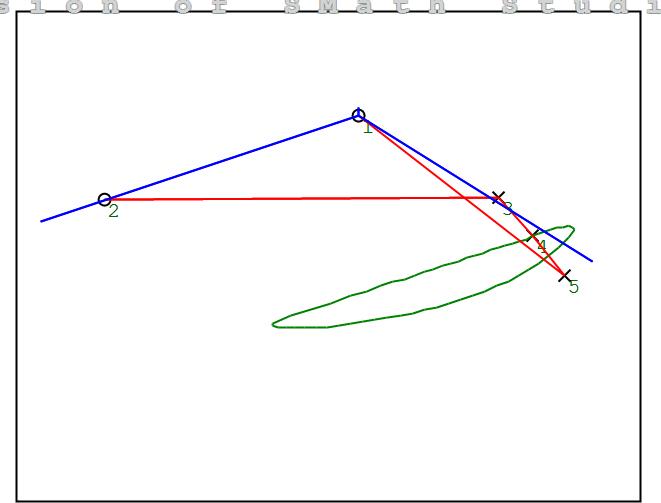


$$Bar4 (a, b, f, g) = \begin{bmatrix} "Inp link a" "θmin" "θmax" "Out link b" "ψmin" "ψmax" \\ "crank" "∅" "∅" "rocker" 70.5288 126.8699 \end{bmatrix}$$

```

Created using a free version of SMath Studio
[ N:=60 n:=[1..(N+1)] θo:=pRR(37°, 103°, N) ]
[ f:=1 a:=5·f b:=5·f g:=4·f zo:=0.1 ]
[ Po:=[ 0 0 0 ] Pg:=[ g b zo ]
[ g 0 0 ] [ f b 0 ]
[ 0 b -zo ]
E:=[ 2 3 4 5 ]
[ 3 4 5 1 ]
[ b f f a ]
BarE(θ, x, y, z):=
[ BarR(θ, x₅, y₅)
  BarA(180°, x, y, 3, 5, 4)
  z₃ - zo
  z₄
  z₅ + zo ]
[ P W]:=BarPW(θo, E, Po, Pg)

```



BarPlot(t, Po, P, W, 4)

$$\text{Bar4}(a, b, 2·f, g) = \begin{bmatrix} \text{"Inp link a"} & \text{"θmin"} & \text{"θmax"} & \text{"Out link b"} & \text{"ψmin"} & \text{"ψmax"} \\ \text{"rocker"} & 36.9 & 101.5 & \text{"rocker"} & 78.5 & 143.1 \end{bmatrix}$$

### Chebyshev Lambda Linkage

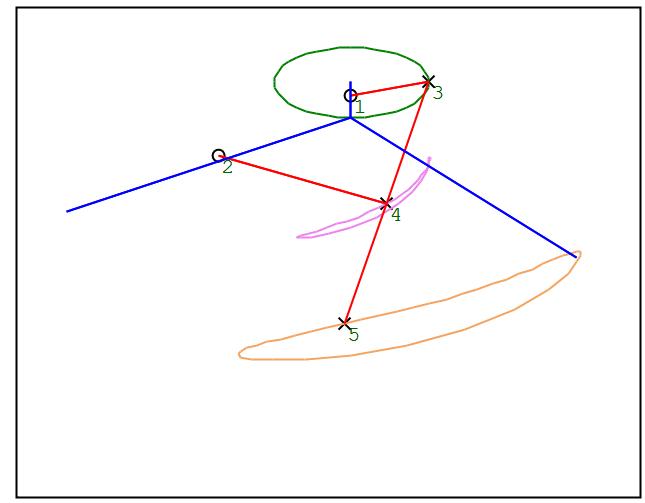
It's a 5 bar based in a previous example of 4 bar.

We introduce also some noise in the node 2 and a small height.

```

[ N:=40 n:=[1..(N+1)] θo:=pR(0, 2·π, N) ]
[ a:=1 zo:=0.3 τ:=t/N ]
[ Po:=[ 0 0 zo ]
  2·a 0.2·sin(2·π·τ) 0 ] Pg:=[ -a 0 0
  0.5·a 2·a 0 ]
  2·a 4·a 0 ]
E:=[ 1 2 3 4
  3 4 4 5
  a 2.5·a 2.5·a 2.5·a ]
BarE(θ, x, y, z):=
[ BarR(θ, x₃, y₃)
  BarA(180°, x, y, 3, 4, 5)
  z₃ - 0.5
  z₄
  z₅ + 0.5 ]
[ P W]:=BarPW(θo, E, Po, Pg)

```



BarPlot(t, Po, P, W)

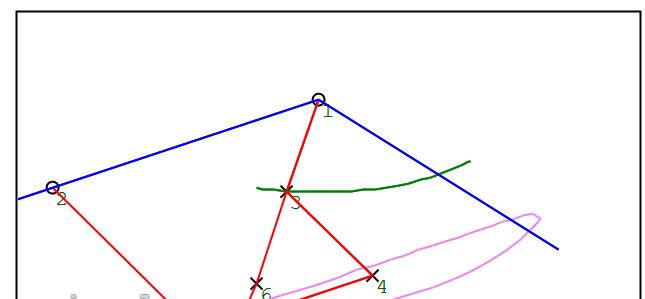
$$\text{Bar4}(a, 2.5·a, 2.5·a, 2·a) = \begin{bmatrix} \text{"Inp link a"} & \text{"θmin"} & \text{"θmax"} & \text{"Out link b"} & \text{"ψmin"} & \text{"ψmax"} \\ \text{"crank"} & \text{"E"} & \text{"E"} & \text{"rocker"} & 78.5 & 143.1 \end{bmatrix}$$

### Chebyshev Table Linkage

```

[ N:=40 n:=[1..(N+1)] θo:=pRR(105°, 35°, N) ]
[ a:=1 b:=5·a g:=4·a ]
[ Po:=[ 0 0 0 ]
  4·a 0 0 ] Pg:=[ 2·a a 0
  2·a 4·a 0 ]
  4·a 4·a 0
  4·a 3·a 0
  4·a 5·a 0 ]

```



Created 2023-03-12 05:29:33 - F:\USERS\Desktop\LinkageBars.pdf  
**version of SMath Studio**

---


$$E := \begin{bmatrix} 3 & 7 & 4 & 5 & 6 & 7 & 6 \\ 2.5 \cdot a & 5 \cdot a & 2.5 \cdot a & 2 \cdot a & a & a & 2.5 \cdot a \end{bmatrix}$$

$$BarE(\theta, x, y, z) := \begin{bmatrix} BarR(\theta, x_3, y_3) \\ BarA(180^\circ, x, y, 1, 3, 6) \\ BarA(180^\circ, x, y, 6, 5, 7) \end{bmatrix}$$

$$[P\ W] := BarPW(\theta_0, E, Po, Pg, "J")$$

— Hoecken linkage —

### Hoecken linkage

This example shows how to implement an sliding joint, using 0 as distance between nodes in the E matrix.

---

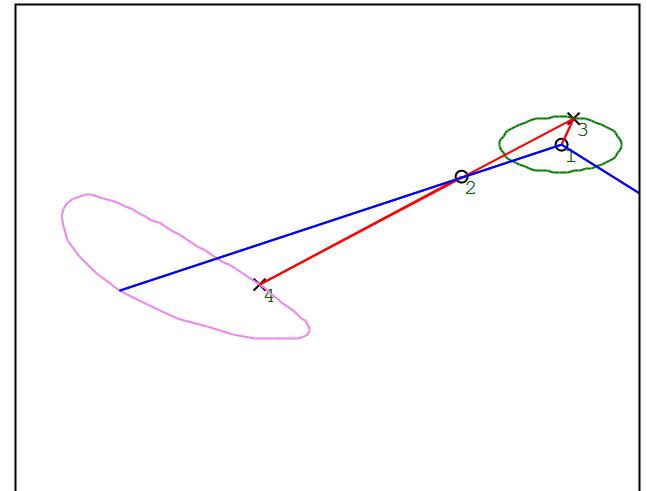

$$[N := 60\ n := [1..(N+1)]\ \theta_0 := pR(0^\circ, 360^\circ, N)]$$

$$[a := 1\ v := 6]$$

$$[Po := \begin{bmatrix} 0 & 0 & 0 \\ 2 \cdot a & 0 & 0 \end{bmatrix}\ Pg := \begin{bmatrix} a & 0 & 0 \\ v \cdot a & 0 & 0 \end{bmatrix}]$$

$$E := \begin{bmatrix} 1 & 3 & 2 \\ 3 & 4 & 4 \\ a & 2 \cdot a + v \cdot a & 0 \end{bmatrix}$$

$$BarE(\theta, x, y, z) := \begin{bmatrix} BarR(\theta, x_3, y_3) \\ BarA(180^\circ, x, y, 3, 2, 4) \end{bmatrix}$$

$$[P\ W] := BarPW(\theta_0, E, Po, Pg)$$


BarPlot(t, Po, P, W)

— Roberts linkage —

### Roberts linkage

It is a four-bar linkage which converts a rotational motion to approximate straight-line motion

---

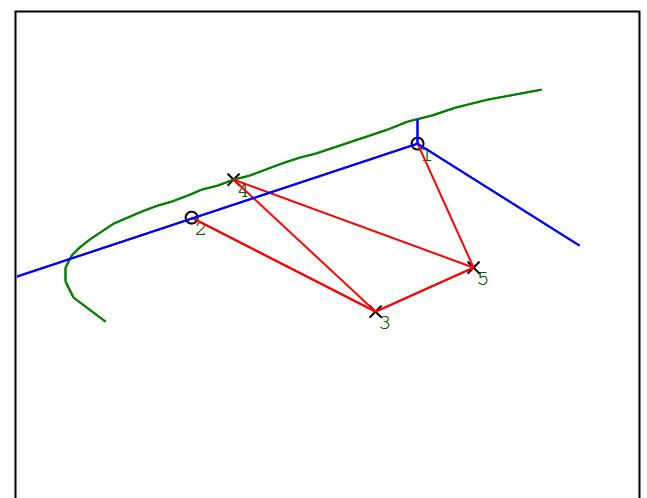

$$[N := 60\ n := [1..(N+1)]\ \theta_0 := pRR(30^\circ, 97^\circ, N)]$$

$$[a := 2\ b := 1\ zo := 0.2]$$

$$[Po := \begin{bmatrix} 0 & 0 & 0 \\ 2 \cdot b & 0 & 0 \end{bmatrix}\ Pg := \begin{bmatrix} 3 \cdot b & a & 0 \\ b & 0 & zo \\ 0.5 \cdot b & a & 0 \end{bmatrix}]$$

$$E := \begin{bmatrix} 2 & 3 & 4 & 5 & 3 \\ 3 & 4 & 5 & 1 & 5 \\ a & a & a & a & b \end{bmatrix}$$

$$BarE(\theta, x, y, z) := \begin{bmatrix} BarR(\theta, x_5, y_5) \\ z_3 \\ z_4 - zo \\ z_5 \end{bmatrix}$$

$$[P\ W] := BarPW(\theta_0, E, Po, Pg)$$


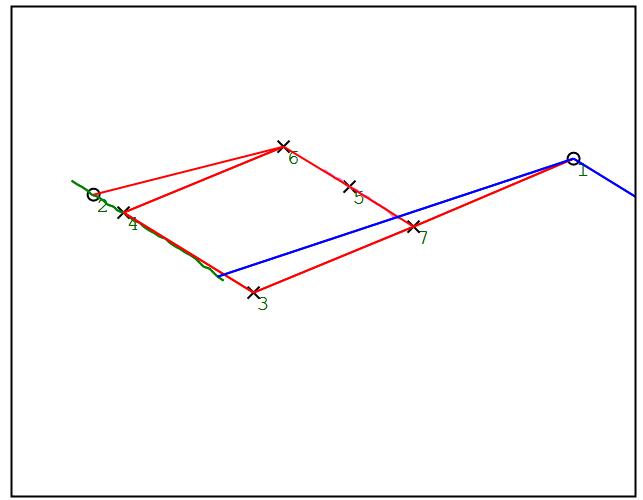
BarPlot(t, Po, P, W, 4)

$$Bar4(a, a, b, 2 \cdot b) = \begin{bmatrix} "Inp link a" & "\theta_{min}" & "\theta_{max}" & "Out link b" & "\psi_{min}" & "\psi_{max}" \\ "rocker" & 29.0 & 97.2 & "rocker" & 82.8 & 151.0 \end{bmatrix}$$

**Parallel motion linkage**

It is a six-bar mechanical linkage described by James Watt

$$\begin{aligned} N &:= 60 \quad n := [1..(N+1)] \quad \theta_0 := pRR(-5^\circ, 30^\circ, N) \\ a &:= 2 \quad b := 1 \quad z_0 := 0.0 \\ Po &:= \begin{bmatrix} 0 & 0 & 0 \\ 2 \cdot a & -2 \cdot b & 0 \end{bmatrix} \quad Pg := \begin{bmatrix} 2 \cdot a & 0 & 0 \\ 2 \cdot a & -b & 0 \\ a & -b & 0 \\ a & -2 \cdot b & 0 \\ a & 0 & 0 \end{bmatrix} \\ E &:= \begin{bmatrix} 1 & 7 & 3 & 7 & 5 & 4 & 6 \\ 7 & 3 & 4 & 5 & 6 & 6 & 2 \\ a & a & 2 \cdot b & b & b & a & a \end{bmatrix} \\ BarE(\theta, x, y, z) &:= \begin{bmatrix} BarR(\theta, x_7, y_7) \\ BarA(180^\circ, x, y, 1, 7, 3) \\ BarA(180^\circ, x, y, 7, 5, 6) \end{bmatrix} \\ [P \ W] &:= BarPW(\theta_0, E, Po, Pg) \end{aligned}$$



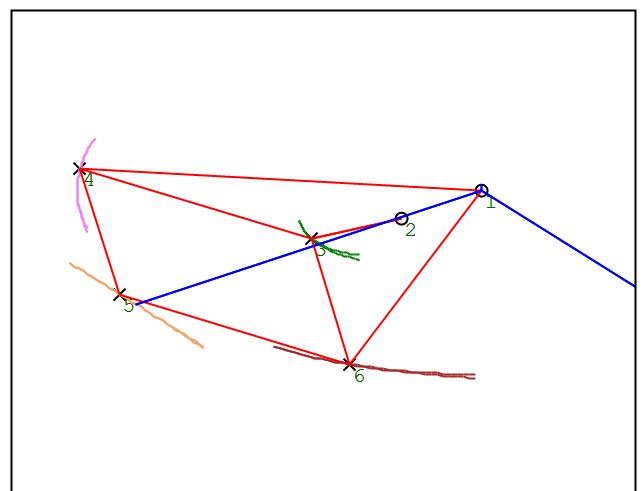
BarPlot(t, Po, Pg, [4 5])

## ■—Peaucellier–Lipkin linkage

**Peaucellier–Lipkin linkage**

It is the first true planar straight line mechanism.

$$\begin{aligned} N &:= 60 \quad n := [1..(N+1)] \quad \theta_0 := pRR(30^\circ, -30^\circ, N) \\ a &:= 0.8 \quad b := 2.2 \quad c := 3.2 \quad z_0 := 0.0 \\ Po &:= \begin{bmatrix} 0 & 0 & 0 \\ a & 0 & 0 \end{bmatrix} \quad Pg := \begin{bmatrix} 2 \cdot a & a & 0 \\ c & 0 & 0 \\ 2 \cdot c & b & 0 \\ c + b & 2 \cdot b & 0 \end{bmatrix} \\ E &:= \begin{bmatrix} 1 & 1 & 2 & 3 & 4 & 5 & 6 \\ 6 & 4 & 3 & 4 & 5 & 6 & 3 \\ c & c & a & b & b & b & b \end{bmatrix} \\ BarE(\theta, x, y, z) &:= \begin{bmatrix} BarR(\theta, x_3 - a, y_3) \end{bmatrix} \\ [P \ W] &:= BarPW(\theta_0, E, Po, Pg) \end{aligned}$$



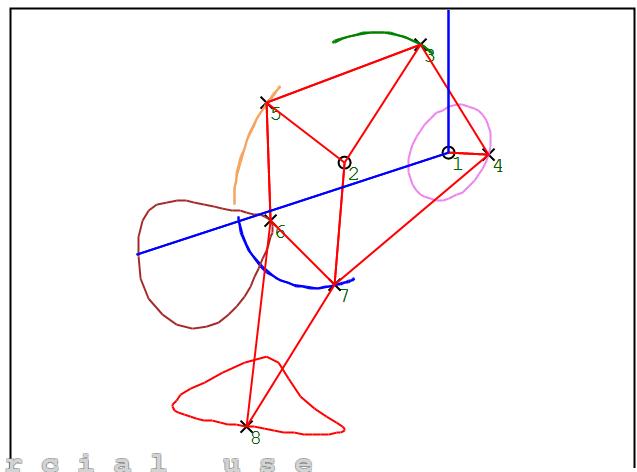
BarPlot(t, Po, Pg)

## ■—Jansen's linkage

**Jansen's linkage**It is a planar leg mechanism. Here we use the option "J" for the solver.  
Values are from <https://github.com/cvigoie/Jansen/blob/master/jansen.pdf>

$$\begin{aligned} N &:= 40 \quad n := [1..(N+1)] \quad \theta_0 := pR(0^\circ, 360^\circ, N) \\ k_{32} &:= 4.15 \quad k_{27} := 3.93 \quad k_{25} := 4.01 \quad k_{35} := 5.58 \\ k_{56} &:= 3.94 \quad k_{67} := 3.67 \quad k_{68} := 6.57 \quad k_{78} := 4.90 \\ k_{34} &:= 5.00 \quad k_{47} := 6.19 \quad k_{14} := 1.50 \quad \lambda := 0.78 \quad a := 3.80 \\ Po &:= \begin{bmatrix} 0 & 0 & 0 \\ a & 0 & \lambda \end{bmatrix} \quad Pg := \begin{bmatrix} k_{14} & 0 & k_{34} \\ -k_{34} & 0 & 0 \\ a + k_{25} & 0 & \lambda \\ a + k_{25} & 0 & -\lambda \\ a & 0 & -k_{27} \end{bmatrix} \end{aligned}$$

Not for commercial use

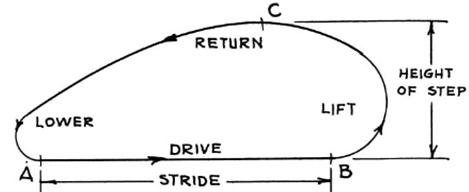


BarPlot(t, Po, P, W)

$$E := \begin{bmatrix} 2 & 4 & 4 & 3 & 3 & 2 & 5 & 6 & 6 & 7 & 1 \\ 5 & 3 & 7 & 2 & 5 & 7 & 6 & 7 & 8 & 8 & 4 \\ k_{25} & k_{34} & k_{47} & k_{32} & k_{35} & k_{27} & k_{56} & k_{67} & k_{68} & k_{78} & k_{14} \end{bmatrix}$$

$$\text{BarE}(\theta, x, y, z) := \left[ \text{BarR}(\theta, x_4, z_4) \right]$$

$$[P\ W] := \text{BarPW}(\theta_0, E, Po, Pg, "J")$$

Shigley's  
Phases of the  
Foot-Path

□—Trammel of Archimedes

**Trammel of Archimedes**

This example shows how to move a 'fixed' node, using the special variable t, which is the variable in the SMath plots for animations (the range is given by n).

Another way to do that is

$$\tau := \frac{t - 1}{N}$$

$$Po := [0 \ 2 \cdot b \cdot \sin(2 \cdot \pi \cdot \tau) \ 0]$$

Usually, the trammel have only one node, but here we add 3.  
The last equation in BarE is for force x2 to change the sign.

$$N := 40 \ n := [1 .. (N + 1)] \ \theta_0 := pR(0, 2 \cdot \pi, N)$$

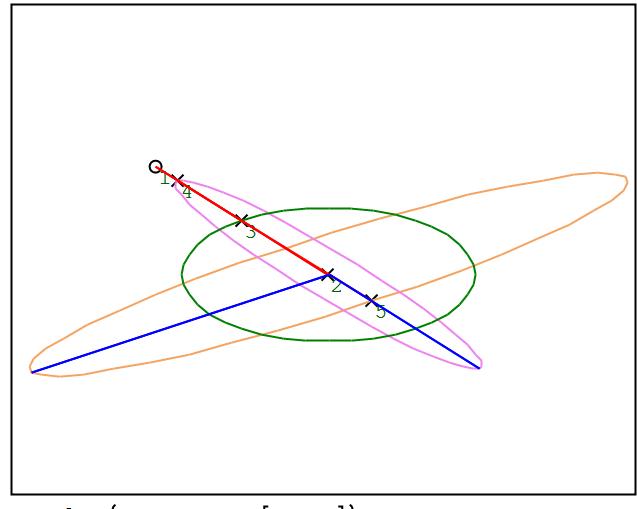
$$a := 2$$

$$Po := [0 \ 2 \cdot a \cdot \sin(\theta_0 \ t) \ 0] \ Pg := \begin{bmatrix} 2 \cdot a & 0 & 0 \\ a & 0 & 0 \\ 0.75 \cdot a & 0 & 0 \\ 1.5 \cdot a & 0 & 0 \end{bmatrix}$$

$$E := \text{eval} \begin{bmatrix} 1 & 2 & 3 & 3 \\ 3 & 3 & 4 & 5 \\ a & a & 0.75 \cdot a & 1.5 \cdot a \end{bmatrix}$$

$$\text{BarE}(\theta, x, y, z) := \begin{bmatrix} \text{BarA}(0^\circ, x, y, 2, 1, 3) \\ \text{BarA}(0^\circ, x, y, 2, 4, 3) \\ \text{BarA}(0^\circ, x, y, 2, 5, 3) \\ x_2 - 2 \cdot a \cdot \cos(\theta) \end{bmatrix}$$

$$[P\ W] := \text{BarPW}(\theta_0, E, Po, Pg)$$

**Variation in 3D**

$$N := 40 \ n := [1 .. (N + 1)] \ \theta_0 := pR(0^\circ, 360^\circ, N)$$

$$\tau := \frac{t - 1}{N}$$

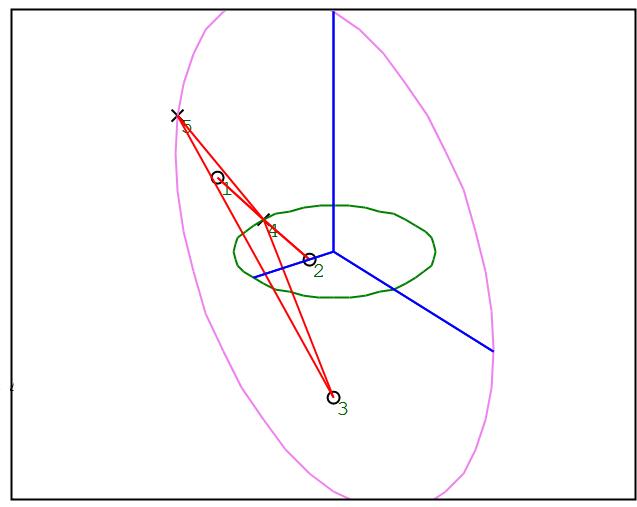
$$a := 3 \ c := a \ k := 1 \ \kappa := \left| \frac{1}{\cos(-45^\circ)} \right| \ b := \frac{2 \cdot a}{\kappa}$$

$$b := 4$$

$$Po := \begin{bmatrix} 0 & 2 \cdot a \cdot \sin(\theta_0 \ t) & 0 \\ 2 \cdot a \cdot \cos(\theta_0 \ t) & 0 & 0 \\ 0 & 0 & -2 \cdot b \end{bmatrix}$$

$$Pg := \begin{bmatrix} a & 0 & 0 \\ 0 & 0 & -2 \cdot b \end{bmatrix}$$

$$E := \begin{bmatrix} 1 & 2 & 3 & 3 & 4 \\ 4 & 4 & 4 & 5 & 5 \\ a & a & 0 & 0 & 0 \end{bmatrix}$$



Created using a free version of SMaTh Studio

$$\begin{aligned} BarE(\theta, x, y, z) := & \begin{pmatrix} y_5 - 2.b \cdot \sin(\theta - 0^\circ) \\ z_5 - 2.b \cdot \cos(\theta - 0^\circ) \\ x_5 \end{pmatrix} \\ [P\ W] := & BarPW(\theta_0, E, Po, Pg, "J") \end{aligned}$$


---

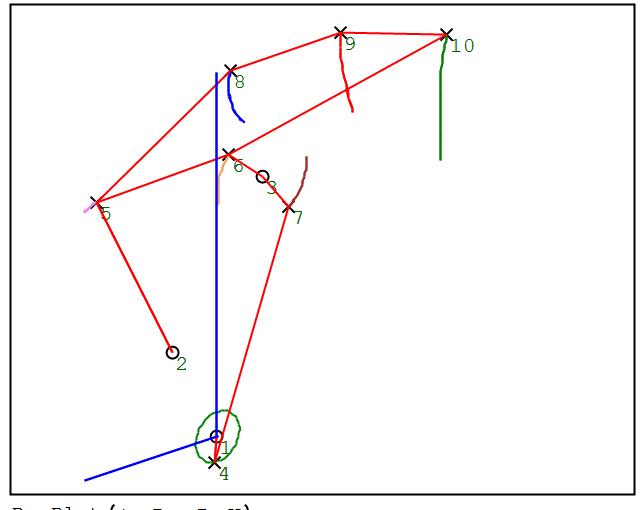
□—Sewing machine —

### Sewing machine

Just trial and error for get some stable lenghts.

$$\begin{aligned} N := 40 \quad n := [1..(N+1)] \quad \theta_0 := pR(0, 2\cdot\pi, N) \\ Po := \begin{bmatrix} 0 & 0 & 0 \\ 1 & 0 & 2 \\ -1 & 0 & 5 \end{bmatrix} \quad Pg := \begin{bmatrix} 0.5 & 0 & 0 \\ 3 & 0 & 5.5 \\ 0 & 0 & 5.5 \\ -2 & 0 & 5.5 \\ 1 & 0 & 7.5 \\ -2 & 0 & 8 \\ -4 & 0 & 10 \end{bmatrix} \\ E := \begin{bmatrix} 1 & 2 & 5 & 5 & 6 & 7 & 6 & 8 & 9 & 4 \\ 4 & 5 & 8 & 6 & 3 & 3 & 10 & 9 & 10 & 7 \\ 0.5 & 4 & 3.5 & 3 & 1 & 1 & 5 & 2.5 & 2.5 & 5 \end{bmatrix} \\ BarE(\theta, x, y, z) := \begin{pmatrix} BarR(\theta, x_4, z_4) \\ BarA(170^\circ, x, z, 6, 3, 7) \\ BarA(170^\circ, x, z, 10, 6, 5) \\ y_4 \end{pmatrix} \\ [P\ W] := BarPW(\theta_0, E, Po, Pg) \end{aligned}$$


---



Alvaro