

Material and Thickness Selection

REDUCTION WITHOUT KNUCKLE CALCULATIONS

DESIGN PARAMETERS

Material : "S235JR"

Tensile Strength : $\sigma_u = 360 \text{ MPa}$

Yield Strength : $\sigma_y = 235 \text{ MPa}$

Safety Factor : $S := 1.5$

Design Strength : $f := \frac{\sigma_y}{S} = 156.667 \text{ MPa}$

Inside Pressure : $P_i := 8 \text{ bar}$

Outside Pressure : $P_e := 2 \text{ bar}$

Welding Factor : $z := 0.85$

Corrosion Allowance : $c = 2 \text{ mm}$

REDUCTION DIMENSIONS

Inlet Inside Diameter : $D_i := 2900 \text{ mm}$

Outlet Inside Diameter : $D_o := 1800 \text{ mm}$

Reduction Length : $L := 3000 \text{ mm}$

Plate Thickness : $e_d = 12 \text{ mm}$

Plate Thickness Calculation

Cone Thickness

$e_a := e_d - c = 10 \text{ mm}$

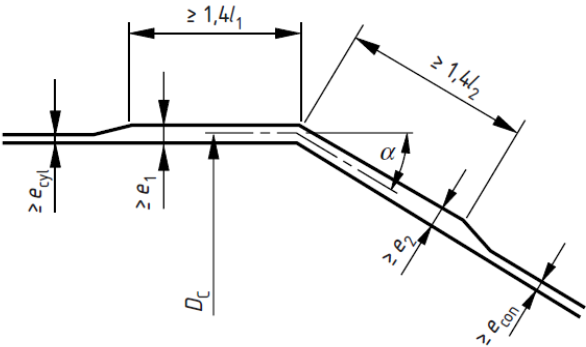
$\alpha := \text{atan}\left(\frac{D_i - D_o}{2 \cdot L}\right) = 10.3889^\circ$

$e_{cyl} := \frac{P_i \cdot D_i}{2 \cdot f \cdot z - P_i} = 8.74 \text{ mm}$

$e_{con} := \frac{P_i \cdot D_i}{2 \cdot f \cdot z - P_i} \cdot \frac{1}{\cos(\alpha)} = 8.88 \text{ mm}$

$e_{min_cyl} := e_{cyl} + c = 10.74 \text{ mm}$

$e_{min} := e_{con} + c = 10.88 \text{ mm}$



$\sigma_a := \frac{P_i \cdot D_i}{2 \cdot \cos(\alpha) \cdot (e_a) \cdot z} = 138.75 \text{ MPa}$

Sanity Checks

$$e_{con} < e_a = 1$$

Safe

$$\sigma_a < f = 1$$

Safe

$$\alpha \leq 75^\circ = 1$$

Check

$$\frac{e_a \cdot \cos(\alpha)}{(D_c := D_i + e_a)} \geq 0.001 = 1$$

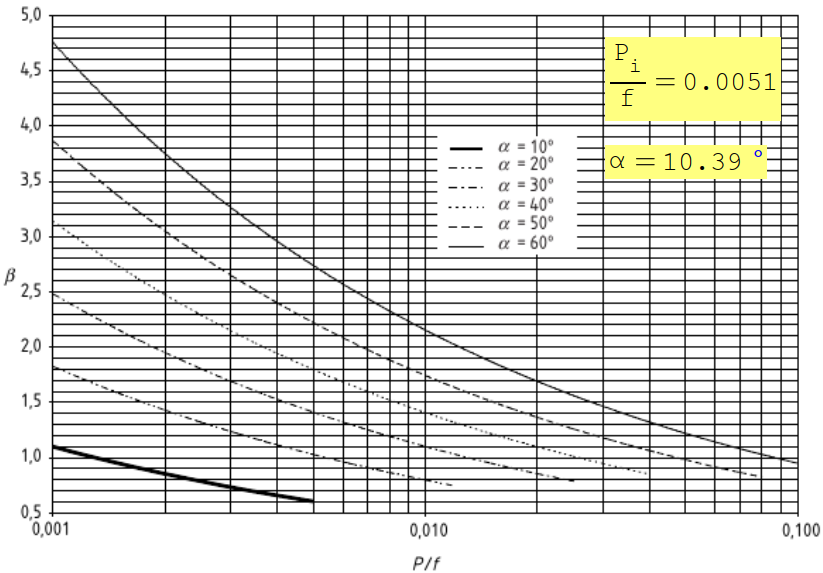
Check

Joint without Knuckle Calculations

$$\beta := \frac{1}{3} \cdot \sqrt{\frac{D_c}{e_j}} \cdot \frac{\tan(\alpha)}{1 + \frac{1}{\sqrt{\cos(\alpha)}}} - 0.15$$
$$e_j := \frac{P_i \cdot D_c \cdot \beta}{2 \cdot f}$$

beta iteration

```
f_Δ(x ; y) := |y - x| / x
e_j := e_con
Δ := 1
while Δ > 0.00001
  D_c := D_i + e_j
  e_temp := e_j
  β := 1/3 * sqrt(D_c / e_j) * tan(α) / (1 + 1/sqrt(cos(α))) - 0.15
  e_j := (P_i * D_c * β) / (2 * f)
  Δ := f_Δ(e_j ; e_temp)
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$\beta = 0.6168$

$e_j = 4.57 \text{ mm}$

$e_1 := \text{Max}(e_{cyl} ; e_j) + c = 10.74 \text{ mm}$

$e_2 := \text{Max}(e_{con} ; e_j) + c = 10.88 \text{ mm}$

$D_c := D_i + e_1$

$l_1 := \sqrt{D_c \cdot e_1} = 176.79 \text{ mm}$

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$l_1 \cdot 1.4 = 247.5 \text{ mm}$

$D_c := D_i + e_2$

$l_2 := \sqrt{\frac{D_c \cdot e_2}{\cos(\alpha)}} = 179.46 \text{ mm}$

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$l_2 \cdot 1.4 = 251.25 \text{ mm}$